

User's Reference Manual for a Three-Dimensional Numerical Hydrodynamic and Transport Model of the New York Bight

by S. Rao Vemulakonda



Approved For Public Release; Distribution is Unlimited

19950821 012

The contents of this report are not to be used for advertising, publication, or promotional purposes. Citation of trade names does not constitute an official endorsement or approval of the use of such commercial products.

User's Reference Manual for a Three-Dimensional Numerical Hydrodynamic and Transport Model of the New York Bight

by S. Rao Vemulakonda

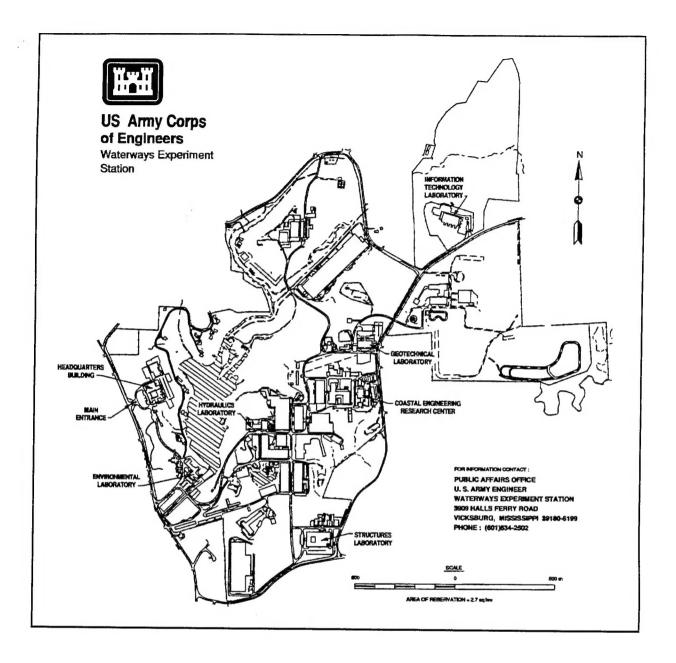
U.S. Army Corps of Engineers Waterways Experiment Station 3909 Halls Ferry Road Vicksburg, MS 39180-6199

Accesion For		
NTIS CRA&I DTIC TAB Unannounced Justification		
By		
Availability Codes		
Dist	Avail ar Spec	
A-1		

Final report

Approved for public release; distribution is unlimited

DTIC QUALITY INSPECTED 2



Waterways Experiment Station Cataloging-in-Publication Data

Vemulakonda, S. Rao.

User's reference manual for a three-dimensional numerical hydrodynamic and transport model of the New York Bight / by S. Rao Vemulakonda; prepared for U.S. Army Engineer District, New York. 82 p.: ill.; 28 cm. — (Instruction report; CERC-95-2)

Includes bibliographic references.

1. Harbors — Hydrodynamics — Mathematical models. 2. Water quality — New York Bight (N.J. and N.Y.) — Mathematical models. 3. Hydrodynamics — Mathematical models — Handbooks, manuals, etc. I. United States. Army. Corps of Engineers. New York District. II. U.S. Army Engineer Waterways Experiment Station. III. Coastal Engineering Research Center (U.S. Army Engineer Waterways Experiment Station) IV. Title. V. Series: Instruction report (U.S. Army Engineer Waterways Experiment Station); CERC-95-2. TA7 W34i no.CERC-95-2

Contents

Preface
Conversion Factors
1—Introduction
2—CH3D-WES Hydrodynamic Model
2—CH3D-WES Hydrodynamic Model
Governing Equations
Non-Dimensionalization of Equations
External-Internal Modes
Boundary-Fitted Equations
Boundary Conditions
Initial Conditions
Numerical Solution Algorithm
Turbulence Parameterization
Computational Grid
Computational Grid
3—Structure of the New York Bight 3D Hydrodynamic Model 15
4—Demonstration of the Setup of Input Files
INCLUDE Files
Basic Control Data
Freshwater Inflows
Wind Speed
Grid Coordinates and Water Depths
Tabular Tides
Initial Townsentons and Calindry
Initial Temperature and Salinity
Surface Heat Exchange Information
Tidal Boundary Salinity and Temperature
River Temperature
River Temperature 26 5—Summary 27
River Temperature

Appendix	B: List of Input Data in File 4
Appendix	C: List of Input Data Files
	D: Input Data in File 4 for April 1976
Appendix	E: River Inflows in File 13 E
Appendix	F: Wind Data in File 14
Appendix	G: Cell Corner Coordinates and Depths in File 15
Appendix	H: Tabular Tide in File 16 H
Appendix	I: Initial Temperature Field in File 17
	J: Equilibrium Temperature and Surface Heat ge Coefficient in File 19
Appendix and Ten	K: Time-Varying Vertical Distributions of Salinity nperature at the Ocean Boundary in File 76
	L: Time-Varying Vertical Distribution of Temperature iver Boundary in File 78
SF 298	
List of	Figures
Figure 1.	The New York Bight study area
Figure 2.	New York Bight computational grid
Figure 3.	Sigma-stretched grid
Figure 4.	Staggered grid
Figure 5.	Typical values of NS and MS for different cell

Preface

The hydrodynamic modeling work described in this report was a part of the New York Bight Hydro-Environmental Modeling and Monitoring Study, authorized under Section 728 of the Water Resources Act of 1986. The study was performed during 1989-1993 for the U.S. Army Engineer District, New York (CENAN) by the U.S. Army Engineer Waterways Experiment Station (WES).

Hydrodynamic modeling was performed by personnel of the Coastal Engineering Research Center (CERC) of WES, under the general supervision of Dr. James R. Houston and Mr. Charles C. Calhoun, Jr., Director and Assistant Director, respectively, of CERC. Direct supervision was provided by Mr. H. Lee Butler, Chief of the Research Division (RD), CERC, and overall WES Manager of the New York Bight project, Mr. Bruce A. Ebersole, Chief of the Coastal Processes Branch, RD, CERC, and Dr. Martin C. Miller, Chief of the Oceanography Branch, RD, CERC.

This report was prepared during 1993 by Dr. S. Rao Vemulakonda of CERC, and draws heavily on an earlier user's guide for the Chesapeake Bay hydrodynamic model (Johnson et al. 1991b).

CENAN points of contact during the study were Mr. John Tavalero, Ms. Patricia Barnwell-Pechko, Ms. Lynn Bocamazo, and Mr. Bryce Wisemiller. Their direction and assistance were invaluable. Field data for the 1975-1976 period were collected under the Marine EcoSystem Analysis (MESA) program and were made available under contract to WES by Dr. Andrew Stoddard of Creative Enterprises of Northern Virginia, Inc., and Dr. Gregory Han of Han & Associates, Inc.

At the time of publication of this report, Director of WES was Dr. Robert W. Whalin. Commander was COL Bruce K. Howard, EN.

The contents of this report are not to be used for advertising, publication, or promotional purposes. Citation of trade names does not constitute an official endorsement or approval of the use of such commercial products.

Conversion Factors, NON-SI to SI Units of Measurement

Non-SI units of measurement used in this report can be converted to SI units as follows:

Multiply	Ву	To Obtain
cubic feet/sec	0.02831685	cubic meters/sec
feet	0.3048	meters

1 Introduction

The New York Bight (NY Bight, Figure 1) is generally considered to be the area of the Atlantic Ocean extending from Cape May, New Jersey to Montauk Point, New York. Laterally, the NY Bight extends about 160 km from the coastline to the continental shelf break. It is a part of the Middle Atlantic Bight. Depths in the region vary from 3 m near Sandy Hook, New Jersey to 900 m in the Hudson Canyon, to over 2,000 m seaward of the continental shelf. Average depths are approximately 60 m. Circulation of water in the NY Bight is influenced by astronomical tides, meteorological forcing, flow from the Hudson-Raritan Estuaries, density gradients due to salinity and temperature variations, and bathymetric variations. Large-scale oceanic processes affecting the entire Middle Atlantic Bight may also play a role.

The NY Bight is of great importance for a variety of reasons, including navigation, recreation, seafood, and disposal of wastes and dredged materials. The adjacent coastal states are heavily populated and urbanized. With increasing population and industrialization come increasing pressures on the ecosystem. The environmental health and productivity of the NY Bight and the potential impacts of natural events and man-made projects on the Bight are therefore of great concern.

This report is a product of the NY Bight Study. The goal of this feasibility study, authorized under Section 728 of the Water Resources Act of 1986, was to identify a means of developing a comprehensive tool for effectively managing the resources of the NY Bight. A combined hydrodynamic-environmental modeling technique, used together with a monitoring plan and a geographic information system, was identified as the preferred approach to determine potential impacts to the NY Bight. This approach was adopted and its feasibility was demonstrated during the course of the study.

Since hydrodynamics is crucial to studying other aspects such as water quality, the three-dimensional hydrodynamic model CH3D-WES (Curvilinear Hydrodynamics in Three Dimensions) was selected for the NY Bight Study. This model was used previously by the Corps of Engineers and the Environmental Protection Agency in a highly successful joint study of the Chesapeake Bay (Johnson et al. 1991a). The model is capable of using a

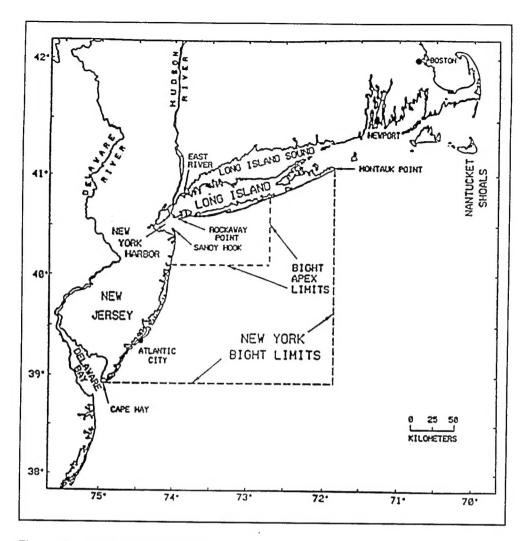


Figure 1. The New York Bight study area

boundary-fitted curvilinear grid in the horizontal to represent complex geometries. In the Chesapeake Bay application, a horizontal (z-) layer approach was used in the vertical direction. Compared to Chesapeake Bay, depths in the NY Bight vary considerably. Therefore, a sigma-layer version of the model was used. In this approach, the same number of layers are used in the vertical direction, in both deep and shallow parts of the study area. Because each sigma layer represents the same fraction of the total depth at a given location, sigma layers are curved. Even though the main interest of the study was in the Outer Bight, Long Island Sound and a part of the New York Harbor were included in the study area and numerical grid for the sake of completeness and to represent the hydrodynamic connections between the three areas.

The numerical grid selected for the study (Figure 2) has high resolution in areas of greater interest. It contains a maximum of 76 cells in the alongshore direction and 45 cells in the cross-shore direction. A total of 2,652 active horizontal (water) cells are used. The average horizontal grid resolution is

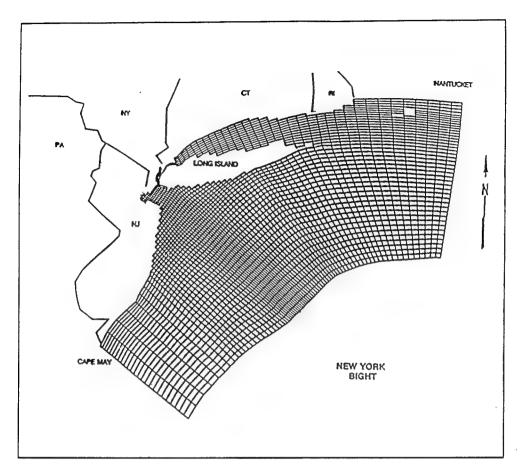


Figure 2. New York Bight computational grid

8 km in the alongshore direction with a minimum of 2 km in the Hudson Canyon and a maximum of 17 km near Cape May. Average resolution in the cross-shore direction is 6 km with a minimum of 200 m in the East River and a maximum of 8 km near the shelf break. The Hudson River is represented as a two-dimensional laterally-averaged body of water.

The hydrodynamic model was calibrated and verified for April and May 1976, using Marine EcoSystem Analysis (MESA) Program field data for surface elevations and currents. A 6-month-long extended validation was performed for the period April 1 - October 1, 1976, using MESA field data for salinity and temperature. Results from the simulation were used to drive successfully the Water Quality Model for the NY Bight. A demonstration of the hydrodynamic model was performed in Long Island Sound and East River for a 72-day period starting May 9, 1990, using the National Oceanic and Atmospheric Administration's (NOAA) field data on surface elevations, currents, salinity and temperature. All of these efforts are described by Scheffner et al. (1994).

The present report is a user guide to the NY Bight hydrodynamic model and should be used in conjunction with the report by Scheffner et al. (1994), which gives more details of the theory and implementation of the CH3D-WES model, as well as numerical simulations performed and results obtained. The present report follows the following outline. After this introduction, the CH3D-WES model is briefly described in Chapter 2. Chapter 3 describes the structure of the model, the various subroutines used and the function of each. In Chapter 4, the setup of various input files is described, using an application of the New York Bight model as an example. Chapter 5 is a summary of the report. Appendix A gives model parameters and dimensions of various arrays used and Appendix B describes the format for the primary input file. Appendixes C-L give sample input files for the application given in Chapter 4.

2 CH3D-WES Hydrodynamic Model

The numerical hydrodynamic model CH3D-WES (Curvilinear Hydrodynamics in Three Dimensions - WES) was selected to provide detailed hydrodynamic flow field information for input to the water quality or environmental model. For convenience, most of the information on CH3D-WES furnished in this report is reproduced from Johnson et al. (1991b). The basic model (CH3D) was developed by Sheng (1986) for WES, but was extensively modified later in its application to the Chesapeake Bay Study. These modifications have consisted of implementing different basic numerical formulations of the governing equations as well as substantial recoding of the model to provide more efficient computing. As its name implies, CH3D-WES makes hydrodynamic computations on a curvilinear or boundary-fitted planform grid. Physical processes impacting circulation and vertical mixing that are modeled include tides, wind, density effects (salinity and temperature), freshwater inflows, turbulence, and the effect of the earth's rotation.

An adequate representation of the vertical turbulence is crucial to a successful simulation of stratification and destratification. A second-order algebraic turbulence model based upon the assumption of local equilibrium of turbulence is employed. The boundary-fitted coordinate feature of the model provides grid resolution enhancement necessary to adequately represent deep navigation channels and irregular shoreline configurations of the flow system. The curvilinear grid also permits adoption of accurate and economical grid schematization software. The solution algorithm employs an external mode, consisting of vertically averaged equations, which provides a solution for the free surface displacement and unit flow rates in two horizontal coordinate directions for input to the internal mode, which solves the full 3D equations.

Governing Equations

The governing partial differential equations are based on the following assumptions:

- a. The hydrostatic pressure distribution adequately describes the vertical distribution of fluid pressure.
- b. The Boussinesq approximation is appropriate.
- c. The eddy viscosity approach adequately describes turbulent mixing in the flow.

The basic equations for an incompressible fluid in a right-handed Cartesian (x,y,z) coordinate system (Johnson et al. 1991b) are:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0 \tag{1}$$

$$\frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uv}{\partial y} + \frac{\partial uw}{\partial z} = fv - \frac{1}{\rho_o} \frac{\partial p}{\partial x} + \frac{\partial}{\partial x} \left(A_H \frac{\partial u}{\partial x} \right)$$

$$+ \frac{\partial}{\partial y} \left(A_H \frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial z} \left(A_v \frac{\partial u}{\partial z} \right)$$
(2)

$$\frac{\partial v}{\partial t} + \frac{\partial uv}{\partial x} + \frac{\partial v^2}{\partial y} + \frac{\partial vw}{\partial z} = -fu - \frac{1}{\rho_o} \frac{\partial p}{\partial y} + \frac{\partial}{\partial x} \left(A_H \frac{\partial v}{\partial x} \right) + \frac{\partial}{\partial z} \left(A_H \frac{\partial v}{\partial z} \right) + \frac{\partial}{\partial z} \left(A_V \frac{\partial v}{\partial z} \right)$$
(3)

$$\frac{\partial p}{\partial z} = -\rho g \tag{4}$$

$$\frac{\partial T}{\partial t} + \frac{\partial uT}{\partial x} + \frac{\partial vT}{\partial y} + \frac{\partial wT}{\partial z} = \frac{\partial}{\partial x} \left(K_H \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(K_H \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(K_v \frac{\partial T}{\partial z} \right)$$
(5)

$$\frac{\partial S}{\partial t} + \frac{\partial uS}{\partial x} + \frac{\partial vS}{\partial y} + \frac{\partial wS}{\partial z} = \frac{\partial}{\partial x} \left(K_H \frac{\partial S}{\partial x} \right) + \frac{\partial}{\partial y} \left(K_H \frac{\partial S}{\partial y} \right) + \frac{\partial}{\partial z} \left(K_y \frac{\partial S}{\partial z} \right)$$
(6)

$$\rho = \rho \ (T,S) \tag{7}$$

where

(u,v,w) = velocities in (x,y,z) directions

t = time

 $f = \text{Coriolis parameter defined as } 2\Omega \sin \phi$

 Ω = rotational speed of the earth

 ϕ = latitude

 ρ = local fluid density

p = local fluid pressure

 $A_{H}K_{H}$ = horizontal turbulent eddy coefficients

 $A_{\nu}K_{\nu}$ = vertical turbulent eddy coefficients

g = gravitational acceleration

T = temperature

S = salinity

 ρ_0 = average (reference) fluid density

Equation 4 implies that vertical accelerations are negligible and thus the pressure is hydrostatic. Equation 7, commonly known as the equation of state, relates the local density to the local temperature and salinity. In practice various forms of the equation can be specified. In the present model, the formulation given below is used:

$$\rho = P/(\alpha + 0.698P) \tag{8}$$

where

 ρ = density in grams per cubic centimeter

$$P = 5890 + 38T - 0.375T^2 + 3S$$

$$\alpha = 1779.5 + 11.25T - 0.0745T^2 - (3.8 + 0.01T)S$$

and T is temperature in degrees Celsius and S is salinity in parts per thousand (ppt).

Non-Dimensionalization of Equations

The dimensionless forms of the governing equations are used to facilitate comparisons of the relative magnitudes of various terms in the governing equations. In what follows, for convenience, the same symbols as before are used to represent dimensionless variables.

External-Internal Modes

For computational efficiency, the solution scheme employs a "mode splitting" technique. In this procedure, Equations 1-4 are integrated over depth to yield a set of vertically integrated equations for the water surface ζ and unit flow rates U and V in the x and y directions (external mode). Thus, the time step for the rapidly varying external mode solution is limited by the surface gravity wave speed (the Courant condition). The major purpose of the external mode is to solve for the updated water-surface field and depth-integrated flows for input to the internal mode equations from which the vertical distributions of velocity, salinity, and temperature fields are computed. The time step for the slowly varying internal mode solutions is thereby removed from the Courant condition restriction and can be much larger than the external mode time step. The two modes together provide the full 3D solution.

Boundary-Fitted Equations

The CH3D-WES model utilizes a boundary-fitted or generalized curvilinear planform grid which can be made to conform to flow boundaries, providing a detailed resolution of the complex horizontal geometry of the flow system. This necessitates the transformation of the governing equations into boundary-fitted coordinates (ξ,η) . If only the (x,y) coordinates are transformed, a system of equations similar to those solved by Johnson (1980) for vertically averaged flow fields is obtained. However, in the CH3D-WES model not only are the (x,y) coordinates transformed into the (ξ,η) curvilinear system but the velocity also is transformed such that its components are contravariant (i.e., perpendicular to the (ξ,η) coordinate lines). This is accomplished by employing the definitions below for the components of the Cartesian velocity (u,v) in terms of contravariant components u and v.

$$u = x_{\xi}\overline{u} + x_{\eta}\overline{v}$$

$$v = y_{\xi}\overline{u} + y_{\eta}\overline{v}$$
(9)

along with the following expressions for replacing Cartesian derivatives

$$f_{x} = \frac{1}{J} [(fy_{\eta})_{\xi} - (fy_{\xi})_{\eta}]$$

$$f_{y} = \frac{1}{J} [-(fx_{\eta})_{\xi} + (fx_{\xi})_{\eta}]$$
(10)

where f is an arbitrary variable and J is the Jacobian of the coordinate transformation defined as

$$J = x_{\xi} y_{\eta} - x_{\eta} y_{\xi}$$

With the governing equations written in terms of the contravariant components of the velocity, boundary conditions can be prescribed on the boundary-fitted grid in the same manner as on a Cartesian grid because \bar{u} and \bar{v} are perpendicular to the curvilinear cell faces (e.g., at a land boundary, either \bar{u} or \bar{v} is set to zero).

The vertical dimension is represented through the use of what is commonly referred to as sigma-stretched grid, illustrated in Figure 3. The vertical depth is discretized in a fixed number of layers, each layer equal in thickness to a fixed percentage of the local depth.

With both the Cartesian coordinates and the Cartesian velocity transformed, boundary-fitted equations for u, v, w, S, and T to be solved in each vertical layer are obtained.

Boundary Conditions

The boundary conditions at the free surface are

$$A_{\nu}\left(\frac{\partial \overline{u}}{\partial z} , \frac{\partial \overline{v}}{\partial z}\right) = \left(\tau_{s_{\xi}}, \tau_{s_{\eta}}\right)/\rho = \left(C W_{\xi}^{2}, C W_{\eta}^{2}\right)$$

$$\frac{\partial T}{\partial z} = \frac{Pr_{\nu}}{E_{\nu}} K (T - T_{e}) \tag{11}$$

$$\frac{\partial S}{\partial z} = 0$$

whereas the boundary conditions at the bottom are

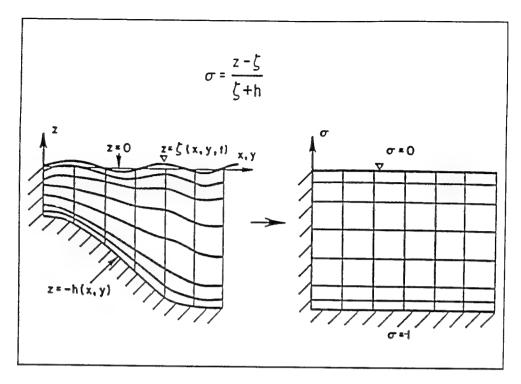


Figure 3. Sigma-stretched grid

$$A_{v} \left(\frac{\partial \overline{u}}{\partial z} , \frac{\partial \overline{v}}{\partial z} \right) = \left(\tau_{b_{t}} , \tau_{b_{v}} \right) / \rho$$

$$\frac{\partial T}{\partial z} , \frac{\partial S}{\partial z} = 0$$
(12)

where

 $\tau_{s\xi}, \tau_{s\eta} = \text{wind stress components}$

 \dot{C} = surface drag coefficient

W =wind speed

 Pr_{ν} = Vertical Prandtl Number

 E_{ν} = Vertical Ekman Number

K =surface heat exchange coefficient

 T_{ϵ} = equilibrium temperature

 $\tau_{b\xi}, \tau_{b\eta}$ = bottom shear stress components

The surface drag coefficient is computed according to Garratt (1977) as follows

$$C = (0.75 + 0.067 W) \times 10^{-3}$$
 (13)

with the maximum allowable value being 0.003. The surface heat exchange coefficient, K, and the equilibrium temperature, T_e , are computed from meteorological data (wind speed, cloud cover, wet and dry bulb air

temperatures, and relative humidity) as discussed by Edinger, Brady, and Geyer (1974).

Freshwater inflow and water temperature are prescribed along the shoreline where river inflow occurs, however, the salinity at the river boundary is specified according to a zero spatial gradient assumption (computed from the previous time step). At an ocean boundary, the water-surface elevation is prescribed along with time-varying vertical distributions of salinity and temperature. Specified values of salinity and temperature are employed during flood flow, whereas during ebb, interior values are advected out of the grid. The normal component of the velocity, the viscosity and diffusivity are set to zero along solid boundaries.

Initial Conditions

When initiating a run of CH3D-WES, the values of ζ , u, v, w, U and V are set to zero. Values of salinity and temperature are read from input files. These initial data are generated from prototype measurements at a limited number of locations. Once the values in individual cells are determined by interpolating from the field data, the resulting 3D field is smoothed. Generally, the salinity and temperature fields are held constant for the first few days of a simulation to allow the flow field solution to spin up.

Numerical Solution Algorithm

Finite differences are used to replace derivatives in the governing equations, resulting in a system of linear algebraic equations to be solved in both the external and internal modes. The external mode solution consists of the surface displacement and vertically integrated contravariant unit flows \bar{U} and \bar{V} . All terms in the transformed vertically averaged continuity equation are treated implicitly whereas only the water-surface slope terms in the transformed vertically averaged momentum equations are treated implicitly. If the external mode is used only as a vertically averaged model, the bottom friction is also treated implicitly. Those terms treated implicitly are weighted between the new and old time-steps. Generally, a typical value of 0.55 for the time-weighting parameter yields stable and accurate solutions. The resulting finite difference equations are then arranged such that a ξ -sweep followed by an η -sweep of the horizontal grid yields the solution at the new time-step.

The internal mode consists of computations for the three velocity components \bar{u} , \bar{v} , and w, salinity, and temperature. The only terms treated implicitly are the vertical diffusion terms in all equations and the bottom friction and surface slope terms in the momentum equations. Values of the water-surface elevations from the external mode are used to evaluate the surface slope terms in the internal mode equations. As a result, the extremely

restrictive speed of a free-surface gravity wave is removed from the stability criteria for the internal mode solution. The second upwind differencing scheme of Roache (1976) is used to represent the convective terms in the momentum equations, whereas a spatially third-order scheme developed by Leonard (1979) (called QUICKEST) is used to represent the advective terms in the transport equations for salinity and temperature.

It should be noted that once the \bar{u} and \bar{v} velocity components are computed, they are slightly adjusted to ensure conservation of mass. This is accomplished by forcing the sum of \bar{u} over the vertical to be the vertically averaged velocity $\bar{U}H$ and the sum of \bar{v} over the vertical to equal $\bar{V}H$, where H is the total water depth.

Turbulence Parameterization

Vertical turbulence is handled by using the concept of eddy viscosity and diffusivity to represent the velocity and density correlation terms that arise from a time averaging of the governing equations. These eddy coefficients are computed from mean flow characteristics using a simplified second-order closure model originally developed by Donaldson (1973). The closure model has been further developed and applied to various types of flows by Lewellen (1977) and Sheng (1982, 1986, 1990). The procedure assumes local equilibrium of turbulence. For more details, the interested reader should refer to these references and to Johnson et al. (1991a).

Computational Grid

A staggered grid (Figure 4) is used in both the horizontal and vertical directions of the computational domain. In the horizontal direction, a unit cell consists of a ζ -point in the center $(\zeta_{i,j})$, a U-point to its "west" $(U_{i,j})$, and a V-point to its "south" $(V_{i,j})$. In the vertical direction, the vertical velocities are computed at the "full" grid points. Horizontal velocities, temperature, salinity, and density are computed at the "half" grid points (half vertical grid spacing below the full points).

Two arrays, NS and MS are set automatically by the model and used to flag the grid cells in the horizontal. The array NS indicates the condition of the "west" and "east" cell boundaries, whereas the array MS denotes the condition of the "north" and "south" cell boundaries (Figure 5).

The boundary-fitted grid shown in Figure 2 was developed to provide a high resolution representation of the complex geometry of the coupled New York Bight, New York Harbor, and Long Island Sound model domain. The computational grid contains a maximum of 76 cells in the alongshore direction and 45 cells in the offshore direction. There are 2,652 active horizontal grid cells and 10 vertical layers, resulting in 26,520 computational cells. The

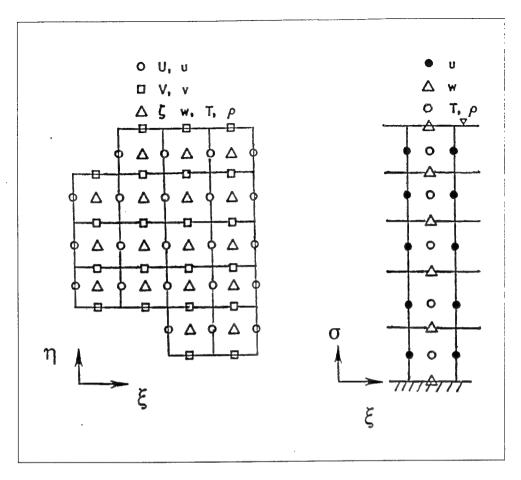


Figure 4. Staggered grid

Hudson river is parameterized as a two-dimensional, laterally-integrated body of water and modeled as a river boundary input to the Bight.

Depths, specified at the cell corners, were extracted from bathymetric data gathered from the National Oceanographic and Atmospheric Administration's (NOAA) nautical charts based on Mean Low Water. Although the resolution in Long Island Sound, New York-New Jersey Harbor and Hudson-Raritan estuary system is coarse for detailed study, the overall grid resolution is sufficient to provide insight into the circulation and transport processes in the Bight.

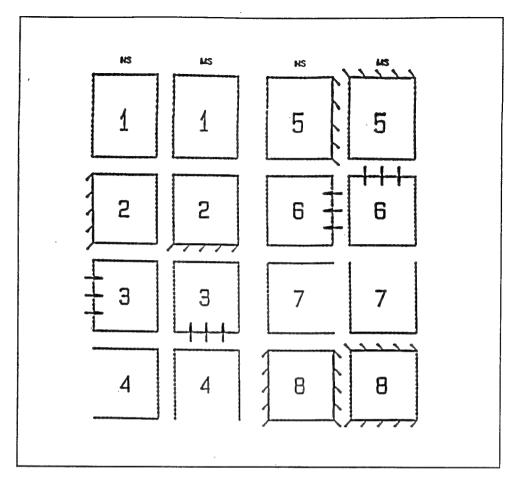


Figure 5. Typical values of NS and MS for different cell boundaries

3 Structure of the New York Bight 3D Hydrodynamic Model

The New York Bight model has a main program as well as several subroutines. Subroutines governing model setup are called from the main program while subroutines governing computations are called from subroutine CH3DM2. Each of these is listed below with a description of its function. Entry points in subroutines are also noted. Note that the UNIX operating system used on the Cray Y-MP computer and the Silicon Graphics' IRIS Indigo Workstation, where the CH3D-WES model is run, is sensitive to lower and upper case letters in file names, commands, etc. Two INCLUDE files, nyb.inc and ch3d.inc, are needed. They are used to set up parameters, dimensions of various arrays, and COMMON blocks. During model compilation, these files are inserted wherever the INCLUDE statements in the source code call for the files. These files are discussed in detail in Chapter 4, along with input files.

CH3D The main program.

CH3DIR Reads data from main input file, FILE 4 (see Appendix B),

which controls computations, input, and output. Various

constants are computed, and the vertical $(\sigma$ -) layer

thicknesses are set.

CH3DTR Reads (x,y) coordinates (ft) and depths (ft) at the cell corners

of the boundary-fitted grid from FILE 15 (ITRAN=2). The coordinates are then multiplied by the scale factor, XMAP, and divided by XREF to make them nondimensional. Subroutine BJINTR is called to provide the coordinate

derivatives needed to compute the metrics of the

transformation.

BJINTR Computes various coordinate derivatives and sets the water

depths HU(I,J) and HV(I,J) on the faces of each

computational cell.

CH3DIH Prints water depths, if requested by input data. Also, the water depths are made nondimensional by dividing by ZREF.

CH3DV1 Sets up flags for different grid cells to indicate land and water for later use in CH3DV2 for flow visualization.

CH3DV3 Similar to CH3DV1 for later use in CH3DV4 for salinity.

CH3DV5 Similar to CH3DV1 for later use in CH3DV6 for temperature.

CH3DND Normalizes several variables and parameters, such as the Eckman number, Rossby number, time-step, etc.

CH3DII Sets up the arrays of boundary flags that indicate the nature of computational cell boundaries. In addition, arrays controlling the computation of the convective terms in the momentum equations and the water surface cross-derivative terms are set up. One-dimensional channel cells are identified.

CH3DIF Initializes various variables for a cold start run and opens time series output files for elevation, velocities, salinity, etc. as well as print and snapshot files. The hot start capability is not operational.

CH3DIV The arrays related to water surface cross-derivatives created in CH3DII, contain logical values. Those arrays are used in this subroutine to create arrays containing numerical values. These arrays, i.e. AFV1(I, J), etc. are used to control computation of not only water surface cross-derivatives but other variables as well.

CH3DWS Controls the reading of either wind speed or wind stress. If the wind speed is read, the stress is computed from Garratt's equation. ENTRY CH3DWT controls the reading of time-varying values and computations.

The subroutines above are called from CH3D in the sequence given. Before calling CH3DM2, which controls the computations, the initial salinity field is read from FILE 74. The initial temperature field is read from FILE 17 and made dimensionless.

CH3DM2 Final subroutine called from CH3D. All subroutines controlling the actual 3D computations are called from this subroutine in the order they appear below.

CH3DDP Computes the total water depths from the latest water surface elevation field. ENTRY CH3DDM sets total water depths at the intermediate time level M and ENTRY CH3DDN sets total water depths at time level N.

CH3DTK Reads equilibrium temperatures and surface heat exchange coefficients from FILE 19 and then transforms them into nondimensional form. ENTRY CH3DTB controls the reading of time-varying values and interpolation.

CH3DRI Reads river inflows from FILE 13. ENTRY CH3DRV controls the reading of time-varying values and interpolation.

CH3DTI Reads and initializes tidal boundary conditions from FILE 16. ENTRY CH3DTD updates boundary values.

CH3DSAI Reads salinities and temperatures at tidal boundaries from FILE 76. ENTRY CH3DSAV controls the reading of time-varying values, interpolation, and conversion to nondimensional form.

CH3DTEI Reads temperatures at river inflow boundaries from FILE 78. ENTRY CH3DTEV controls the reading of time-varying temperatures and interpolation.

WQMOUT This is the main water quality module. It reads information on cell corner points and water quality boxes and computes box lengths, volumes, and flow face areas. ENTRY WQMCVOL computes the volumes for the first time and ENTRY WQTVD computes time-varying information and stores it for later input to the Water Quality Model.

PROC1 This subroutine called by WQMOUT performs Stokes' drift computations.

PTOUT This is the main particle tracking module. It saves time-invariant information on grid characteristics first. ENTRY PTCVOL designates the output file number and ENTRY PTTVD saves time-varying information on wind stress, water depth, surface velocity, horizontal velocity and acceleration, and vertical velocity for later use by the Particle Tracking Model.

EK2, EK2V These subroutines called by PTOUT compute the Ekman drift.

At this point, the loop over time is entered in CH3DM2 and each of the subroutines below is called, usually each time-step.

WOMCVOL ENTRY in WOMOUT for computing initial box volumes.

PTCVOL ENTRY in PTOUT for designating the output file.

CH3DDE Computes water densities using Equation 8. The baroclinic terms in the momentum equations are then evaluated.

CH3DED Sets up arrays that are then used in subroutine CH3DEZ for the computation of eddy viscosity and eddy diffusivity coefficients.

CH3DWT ENTRY in CH3DWS for reading time-varying wind data.

CH3DTB ENTRY in CH3DTK for reading time-varying equilibrium temperature and heat-exchange coefficient.

CH3DRV ENTRY in CH3DRI for reading time-varying river flows.

CH3DTEV ENTRY in CH3DTEI for reading time-varying temperatures at river inflow boundaries.

CH3DTD ENTRY in CH3DTI for reading time-varying tide data.

CH3DSAV ENTRY in CH3DSAI for reading time-varying salinity and temperature profiles at tidal boundaries.

CH3DDN ENTRY in CH3DDP for assigning total water depths at time level N.

CH2DXY Computes the vertically averaged flow field from the vertically averaged equations of motion.

CH3DDP Computes the total water depths at time level N+1, using the water surface field computed in CH2DXY.

CH3DXYZ Computes the 3D velocity field. Mass conservation is ensured by forcing the vertical sum of the horizontal components of the 3D velocity to match the vertically integrated values computed in CH2DXY.

CH3DDI Computes the convective and diffusion terms in the momentum equations using the most recent computation results from CH3DDP and CH3DXYZ. These terms are then employed at the next time step in CH2DXY and CH3DXYZ.

CH3DSA Computes the salinity field.

CH3DTE Computes the temperature field.

CH3DBL Checks the water surface elevations for the program "blowing up".

WOTVD ENTRY in WQMOUT.

PTTVD ENTRY in PTOUT.

CH3DOT Controls the output printed and/or written to files for plotting. Output is in terms of physical dimensional variables. Subroutine CH3DC1 is called with ENTRIES CH3DC2, CH3DC3, CH3DC4, CH3DC5, CH3DC6, CH3DC7, CH3DC8, CH3DC9, CH3DCA, CH3DCC, CH3DCD, and CH3DCE. Each is described below.

CH3DC1 Provides dimensional water surface elevations.

CH3DC2 Provides dimensional physical vertically averaged velocity in x-direction.

CH3DC3 Provides dimensional physical vertically averaged velocity in y-direction.

CH3DC4 Provides dimensional physical horizontal velocity component in x-direction.

CH3DC5 Provides dimensional physical horizontal velocity component in y-direction.

CH3DC6 Provides dimensional physical vertical component of 3D velocity.

CH3DC7 Provides salinity.

CH3DC8 Provides dimensional temperature.

CH3DC9 Provides dimensional physical magnitude and direction of horizontal velocity.

CH3DCA Provides dimensional physical horizontal components of 3D velocity at the centers of cells.

CH3DCC Provides dimensional water density.

CH3DCD Provides dimensional vertical eddy viscosity.

CH3DCE Provides dimensional vertical eddy diffusivity.

After CH3DOT the following subroutines for visualization are called in CH3DM2 in the order shown:

CH3DV2	Saves time-varying flow information.
CH3DV4	Saves time-varying salinity information.
CH3DV6	Saves time-varying temperature information.

In subroutine CH3DOT, the following files are created for use in generating time series plots, vector plots, or contour plots.

FILE 21	For time series plots of dimensional water surface elevation at specified horizontal locations.
FILE 22	For time series plots of dimensional, Cartesian horizontal velocities (x and y directions) at cell centers at specified horizontal locations.
FILE 23	Geometry of study area (needed for plotting snapshots or contours).
FILE 24	For velocity vector plots and contour plots of surface elevation, salinity, temperature, etc.
FILE 25	For time series plots of discharges at specified horizontal ranges.
FILE 31	For time series plots of salinity at specified horizontal locations in all layers.
FILE 34	For time series plots of temperature at specified horizontal locations in all layers.
FILE 35	For time series plots of vertical eddy viscosity at specified horizontal locations in all layers.
FILE 36	For time series plots of vertical eddy diffusivity at specified horizontal locations in all layers.
FILE 37	For time series plots of density at specified horizontal locations in all layers.

The model creates the following additional output files.

FILE 42	For visualization of flow.
FILE 43	For visualization of salinity.
FILE 44	For visualization of temperature.
FILE 70	Geometric data and initial results for particle tracking.
FILE 71	Time-varying data for input to the Particle Tracking Model.
FILE 96	Time-varying data for input to the Water Quality Model.

4 Demonstration of the Setup of Input Files

To demonstrate the setup of input files (see the appendixes), portions of the input files are presented for an application in which the hydrodynamics of the New York Bight during April 1976 was simulated. This application represents the beginning of the long-term (6-month) model validation. Results from this application are presented by Scheffner et al. (1994).

INCLUDE Files

As previously indicated, two INCLUDE files, nyb.inc and ch3d.inc, are needed for compiling the model. Of these, nyb.inc is used to define variable array dimensions in the model for running a particular application, e.g., New York Bight 6-month simulation. It may be necessary for the user to change some of the parameters in nyb.inc. It is listed in Appendix A (page A-1). Parameters, whose values are set in nyb.inc, are used to dimension arrays in COMMON blocks in ch3d.inc and other arrays in the model. All the parameters appearing in nyb.inc are defined below. Of these, ICELLS, JCELLS, IJMAX, and KM have to be set exactly. The others can be greater than or equal to what is needed.

ICELLS : Number of grid cells in the ξ -direction JCELLS : Number of grid cells in the η -direction IJMAX : The greater of ICELLS and JCELLS, plus 1

KM : Number of σ -layers in the vertical

NSTATS : Maximum number of gauge stations where

information will be saved

NTIDES = 11 : Not used

NRIVRS : Number of river boundaries used

NCNST = 37 : Maximum number of tidal constituents used

(set to 37) - used only if tidal signals were generated using constituents - not

operational.

NBNDS : Number of open water boundaries used NBARRS : Number of interior thin-wall barriers

NPRWIN : Number of print windows for printing

model results

NSNAPS : Number of snapshot windows where

information is saved

NRANGS: Number of ranges where discharge

information is saved

NTIDFN: Number of tide functions used NTIDBN: Number of tidal boundaries used

NTIDPT : Maximum number of values in the input

tide functions

NWINDS: Number of input time-varying winds used for

interpolating winds over grid (special for

New York Bight application)

NROWS : Maximum number of computational chains used

in ξ-direction

NCOLS : Maximum number of computational chains used

in η -direction

KROWS : Larger of NROWS and NCOLS, plus 1 NX8PTS : Number of one-cell wide channel cells in

\xi-direction

NY8PTS : Number of one-cell wide channel cells in

n-direction

ISSMAX = 10 : Not used NPLPTS = 75 : Not used NSDMAX = 10 : Not used

SPVAL : A small value to which the vertical eddy

coefficients, etc. are set as a default

In addition, the following parameters are used in connection with the water quality module in CH3D. They should be changed only if the Water Quality Model grid is changed.

NBP : Number of water quality boxes in plan view.

NFP : Number of flow faces in plan view.

A portion of the file ch3d.inc is listed in Appendix A (page A-2). This file does not have to be changed from application to application, but remains the same.

Basic Control Data

Appendix B lists the input variables and their format for the primary input file FILE 4. Appendix C gives a list of all the input files. Input data in FILE 4 for the application mentioned are listed in Appendix D. These data are in response to read statements presented in Appendix B. As can be seen, the computational time-step (DT) is 150 sec with a total of 17,280 time-steps (30 days) simulated (IT2=17280). Both temperature and salinity computations are made (ITEMP= -2 = ISALT), with the initially specified

fields frozen for the first 2,880 time-steps (ITSALT=2880). A time-varying wind (IWIND=5) is specified. There is one river (NRIVER=1), the Hudson. Eight tidal boundaries (TIDBND=8) and eleven tide functions (TIDFNO=11) are used to describe the time-varying tides at the boundaries by linear interpolation.

Freshwater Inflows

Daily-averaged freshwater flows specified at the Hudson River boundary are read from FILE 13. They are given in Appendix E for the first few days of the simulation. Input fields are day, hour, location of the river boundary, and the discharge (cfs).

Wind Speed

Wind data are read from FILE 14. Since IWIND = 5, time-varying wind velocity components (m/sec) are read and wind stresses are computed using Equation 11. For the April 1976 simulation, three wind fields are read (NWINDS = 3). These correspond to hindcast data obtained from three offshore stations of WES Wave Information Study. Inside CH3D-WES, wind velocity components for each computational cell are assigned by linear interpolation from the values read in for the three offshore stations. As can be seen in Appendix F, each line of input in FILE 14 consists of the day, hour, and the x and y components of the wind velocity for each of the three wind stations. Wind data at the three stations are presented in Appendix F only for the first few days in April 1976. Wind stresses computed in the x and y directions are transformed in the model into contravariant components.

Grid Coordinates and Water Depths

The x- and y- coordinates of the cell corners of the computational grid (Figure 2) and the corresponding depths (in feet) are read from FILE 15. The coordinates were generated using the grid generation program EAGLE (Thompson 1987a, 1987b). Landlocked points were assigned coordinate values of 9.0 x 10 18 . Cell water depths were obtained by interpolation from bathymetric data digitized from National Ocean Service nautical charts for the New York Bight region. The format of these data for a few points is illustrated in Appendix G. The first line shows the title and the second line the number of points in the ξ and η directions. The x- and y- coordinates and depth of each point are then input starting with row 1 and moving from left to right, one point per line.

Tabular Tides

The tabular tide data are read from FILE 16. There are 8 tidal boundaries and the tide is interpolated at the boundary cells using 11 tide functions, as defined in the basic input file. Each string of input contains the month, day, year, hour and minute along with the corresponding values of the water surface elevation (cm) at the 11 tidal function point locations. Appendix H illustrates the form of these data for the first few hours of April 1976.

Initial Temperature and Salinity

FILES 17 and 74 are identical in form. FILE 17 contains the initial temperature field, whereas FILE 74 contains the initial salinity field. These files were generated by a computer program which uses a few observed values to assign values to the individual cells in each of the sigma layers. The resulting field is then smoothed in each horizontal direction in each layer and the smoothed field is written to either FILE 17 or FILE 74. Appendix I presents the initial temperature field for sigma layer 1.

Surface Heat Exchange Information

Daily averaged equilibrium temperatures and surface heat exchange coefficients computed from meteorological data at the John F. Kennedy Airport are read from FILE 19. As indicated in Appendix J, each input data line consists of the day and hour since the initiation of the simulation, the equilibrium temperature (deg C), and the surface heat exchange coefficient (cm/sec).

Tidal Boundary Salinity and Temperature

At tidal boundaries, the time-varying vertical distributions of salinity and temperature are read from FILE 76. As illustrated in Appendix K, these data are grouped in the following manner. The day and hour since the initiation of simulation is input on one line. It is followed by a line giving the (I,J) location of the tidal boundary cell and the corresponding vertical salinity distribution. The next line gives the same (I,J) location and the corresponding vertical temperature distribution. These distributions consist of values in each sigma layer, starting with the surface layer and going down to the bottom. This input is repeated for all the tidal boundary cells. Appendix K gives the input for the 61st day of simulation for a few boundary segments. Note information has to be repeated for cells common to two adjacent boundary segments.

River Temperature

River temperature data are read from FILE 78 (APPENDIX L). In the present case, there is only one river boundary, the Hudson. The values are estimated from available U.S. Geological Survey gauging station data. The first line contains the day and hour since initiation of the simulation. Next for each of the NRIVER rivers indicated in the input, the I and J cell indices are given followed by the temperature in different layers, starting from the surface and going down to the bottom. This is done in the order IJRSTR to IJREND for each river. The same procedure is followed for successive times.

5 Summary

The primary purpose of this report is to serve as a user guide for the New York Bight 3D hydrodynamic model. After a brief introduction to the New York Bight study region, the New York Bight feasibility study and the computational grid used, the report describes the main features of the CH3D-WES hydrodynamic model selected for the study. In Chapter 2, the basic governing equations are given followed by the boundary and initial conditions employed.

The report outlines the structure of the computer model in Chapter 3, listing the names of the various subroutines, their functions, and the calling sequence. This should help users who are interested in following the logic of the model. Also listed are various output files created by the model and their contents.

Chapter 4 of the report describes the INCLUDE files needed for defining grid dimensions, COMMON blocks, etc., and discusses the basic control data, and various input files for a specific application for the New York Bight study region covering the month of April 1976. A partial listing of the INCLUDE files is provided in Appendix A. The format of the primary input file is given in Appendix B followed in Appendix C by a list of all the input files required. The user guide function of the report is enhanced by demonstrating the various input files in Appendixes D-L for the specific application.

References

Donaldson, C. dup. 1973. "Atmospheric Turbulence and the Dispersal of Atmospheric Pollutants," *AMS Workshop on Micrometeorology*. D. A. Haugen, ed., Science Press, Boston, 313-390.

Edinger, J. E., Brady, D. K., and Geyer, J. C. 1974. "Heat Exchange and Transport in the Environment," Report 14, EPRI Publication No. 74-049-00-3, Prepared for Electric Power Research Institute, Palo Alto, CA.

Garratt, J. R. 1977. "Review of Drag Coefficients Over Oceans and Continents," *Monthly Weather Review*. Vol 105, 915-929.

Johnson, B. H. 1980. "VAHM - A Vertically Averaged Hydrodynamic Model Using Boundary-Fitted Coordinates," Miscellaneous Paper HL-80-3, U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

Johnson, B. H., Kim, K. W., Heath, R. E., and Butler, H. L. 1991a. "Verification of a Three-Dimensional Numerical Hydrodynamic Model of Chesapeake Bay," Technical Report HL-91-7, U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

Johnson, B. H., Heath, R. E., Hsieh, B. B., Kim, K. W., and Butler, H. L. 1991b. "User's Guide for a Three-dimensional Numerical Hydrodynamic, Salinity, and Temperature Model of Chesapeake Bay," Technical Report HL-91-20, U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

Leonard, B. P. 1979. "A Stable and Accurate Convective Modeling Procedure Based on Upstream Interpolation," *Computer Methods in Applied Mechanics and Engineering*, 19, 59-98.

Lewellen, W.S., 1977, "Use of Invariant Modeling," *Handbook of Turbulence*, W. Frost, ed., Plenum Publishing Corp., 1, 237-280.

Roache, P. J. 1976 "Computational Fluid Dynamics," Hermosa Publishers, Albuquerque, NM.

Scheffner, N. W., Vemulakonda, S. R., Mark, D. J., Butler, H. L., and Kim, K. W. 1994. "New York Bight Study; Report 1, Hydrodynamic Modeling," Technical Report CERC-94-4, U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

Sheng, Y. P. 1982. "Hydraulic Applications of a Second-Order Closure Model of Turbulent Transport," *Applying Research to Hydraulic Practice*, P. Smith, ed., ASCE, 106-119.

Sheng, Y. P. 1986. "A Three-Dimensional Mathematical Model of Coastal, Estuarine and Lake Currents Using Boundary Fitted Grid," Report No. 585, A.R.A.P. Group of Titan Systems, New Jersey, Princeton, NJ, 22.

Sheng, Y. P. 1990. "A Simplified Second Order Closure Model of Turbulent Transport," unpublished paper prepared for the U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

Thompson, Joe F. 1987a. "Program EAGLE - Numerical Grid Generation System User's Manual, Vol 2: Surface Generation System," USAF Armament Laboratory, Eglin Air Force Base, FL.

User's Manual, Vol 3: Grid Generation System," USAF Armament Laboratory, Eglin Air Force Base, FL.

Appendix A Listing of INCLUDE Files

```
INCLUDE FILE FOR NY BIGHT 1993; revised by Rao 7/29/93
      PARAMETER ( IDELLS = 76, JCELLS = 45,
                                             IJHAX = 77)
      PARAMETER ( KH
                        = 10, K1H = KH - 1
      PARAMETER ( NSTATS = 40, NTIDES = 11,
      PARAMETER ( NONST = 37, NBNDS = 11,
                                             NBARRS = 9 )
      PARAMETER ( NPRHIN = 20, NSNAPS = 20,
                                             NRANGS = 20 )
      PARAMETER ( NTIDEN = 12, NTIDEN = 11,
                                             MTIDPT = 10000)
      PARAMETER ( NWINDS = 3
      PARAMETER ( NROWS = 120, NCOLS = 120,
     PARAMETER ( NXBPTS = 10, NYBPTS = 10
     PARAMETER ( IC1 = ICELS + 1, JC1 = JCFLS + 1
     PARAMETER ( IM = ICELLS + 2, JH = JCELLS + 2
     PARAMETER ( ISSNAX = 10.
                                   NPLPTS = 75
     PARAMETER ( NSDHAX = 10,
                                   SPVAL = .1234E-6
Cooses added PARAMETERS from Nater Quality Module ! Rao 7/29/93
Cost Caution: Do not change unless Water Quality Hodel grid changes !!!
     PARAMETER (NBP = 3000, NFP = 6000)
C....
C
```

```
c**** ch3d.inc for NY Bight project: last revised by Rao 7/29/93 - includes
      particle tracking variables; added flags for saving info for water quality
      (IWQ), particle tracking (IPT), and visualization (IVIS).
C -- INCLUDE FILE = CH3D. INC Last revised on 2 MAY 91 KIM
      COMMON /BLK01/ HS(0:IM.0:JH), HU(0:IM.0:JH), HV(0:IM.0:JH),
     1
                      HSD (O: IN. O: JM)
      CONTON /BLX02/ UI (0:1H.0:3H). UIN(0:1H.0:3H). UIN(0:1H.0:3H)
      CONTION /BLKO3/ VI(O:IN.O:JH), VIN(O:IN.O:JH), VIN(O:IN.O:JH)
      CONTION /BLKO4/ S(0:IM.O:JM), SH(0:IM.O:JM), SN(0:IM.O:JM)
C
      COMMON /BLKO5/ AMULIO: IN.O: 3H), AMMINO: IN.O: 3H), AMMINO: IN.O: 3H),
                      ANTO (O: IN.O: JM) . ANTH (O: IN.O: JM) . ANTH (O: IN.O: JM) .
     1
                      AHSS (0: IN. 0: JH) . AHSN (0: IN. 0: JH) . AHSN (0: IN. 0: JH) .
     3
                      AHUI (0:1M.0:3M) - AHVI (0:1M.0:3M) -
                      AHSU(0: IH.O: JH.KH) . AHSV(0: IH.O: JH.KH)
C
      COMMON /BLK07/ AFV1(0:IN.0:JN), AFV2(0:IN.0:JN), AFV3(0:IN.0:JN),
                      AFV4(0:IH.0:JH), AFU1(0:IH.0:JH), AFU2(0:IH.0:JH),
     2
                      AFU3(0:IN.0:JH) - AFU4(0:IN.0:JH)
C
      COMMON /BUX08/ BDSX(IC1.JC1), DDSY(IC1.JC1),
                      DDDX(IC1.JC1), DDDY(IC1.JC1),
     2
                      DHSX(IC1.JC1), DHSY(IC1.JC1),
     3
                      DHTX(IC1.JC1). DHTY(IC1.JC1).
                      DHUX(IC1.JC1), DHUY(IC1.JC1)
C
       CONTION /BLK09/ DIIX(IC1.JC1), DIIY(IC1.JC1)
      COMMON /BLK10/ XD1(IC1, JC1), XD2(IC1, JC1), XD3(IC1, JC1),
                      YD1(IC1,3C1), YD2(IC1,3C1), YD3(IC1,3C1)
       CONTON /BLK11/ RIGHO(0:IM.0:JM.KM). DIRHO(0:IM.0:JM.KM)
       COMMON /BLK12/ THETA
       CONTION /ADD77/ KU, KV
       COMMON /ADD78/ BARLICO: IM.O: JM.KM). BARVICO: IM.O: JM.KM)
       CONTON /BLK16/ XU(IC1), XS(IC1), YV(JC1), YS(JC1), ALXREF, ALYREF
       COMMON /BLK17/ NS(0:IH.0:JH): IROH(NRONS): IUI(NRONS):
                                      ISH (NROHS) . NROH
                      ILIZ (NROWS) .
       CONTION /BLK18/ MS(0:IM.0:JM). JCOL(NCOLS). JV1(NCOLS).
                                      JSH (NCOLS) - NCOL
                       JV2 (NCOLS):
       CONTION /BLKO7A/ KROW(KROWS): KU1(KROWS): KU2(KROWS): KKOL
       COMMON /BLK19/ NR(0:IN:0:JH): MR(0:IN:0:JH)
       COMMON /BLK20/ DT, DIT, DX, DY, DTDX, DTDY, DXI, DYI, D2XI, D2YI,
                      DELT
       COMMON /BLX22/ DEDX(0:IM.0:JM). DEDY(0:IM.0:JM).
                      FIIX(0:IM.0:JM). FIIY(0:IM.0:JM).
      1
      2
                       FHDX (0: IN. 0: JH) - FHDY (0: IN. 0: JH) -
      3
                       CORX(0:IM.0:JM). CORY(0:IM.0:JM).
                       XKOR (0: IN.O: JH.KH) . YKOR (0: IN.O: JH.KH) .
      5
                       TBX(0:1M.0:JM). TBY(0:1M.0:JM). AHO
       CONTIN /BLX23/ IJRDIR(NRIVRS), IJRROW(NRIVRS), IJRSTROWRIVRS),
                       LIREND(NRIVRS), GRIVER(DRIVRS, LIMAX), NRIVER,
      1
      2
                       IDAYA, IHDURA, IDAYB, IHDURS
       COMMON /BLK24/ IJEDIR (NEARRS), IJEROM (NEARRS), IJESTR ONBARRS),
                       IJBEND (NBARRS) . NBAR
       CONTION /BLK25/ IJDIR (NUNDS), IJROM (NUNDS), IJSTRT (NUNDS),
                       IJEND(NENDS), ITIDE, IJLINE, NCG, NCONST
```

```
COMMON /BLK26/ AMPHICICELLS, NTIDES), AMPECICELLS, NTIDES),
                      AMPS (ICELLS, NTIDES), AMPN (ICELLS, NTIDES),
                      PHM (JCELLS: NTIDES) . PHE (JCELLS: NTIDES) .
     2
     3
                      PHS(ICELLS.NTIDES), PHN(ICELLS.NTIDES).
                      CAM (JEELLS, NTIDES), CAE (JCELLS, NTIDES),
                      CAS(ICELLS, NTIDES), CAN(ICELLS, NTIDES),
                      TP(NTIDES)
C
      CONTION /BLK27/ QRIVRA(NRIVRS,IJMAX), QRIVRB(NRIVRS,IJMAX)
      CONTION /BLX28/ IST(NSTATS), JST(NSTATS), NSTA, NFREQ
      CHARACTER+48 STATID, STATSA, STATS
      CONTON /BLX29/ STATIB(NSTATS), STATSA(NSTATS), STATS(NSTATS)
      CONTION /BUX30/ ITERX(10), RSPAC(10), ISPAC(10), JSPAC(10),
                      ITBRK1. ITBRKI
      COHHON /BLX31/ ITRAN, IBD
      COMMON /BLK32/ TX(0:IN.0:JM), TY(0:IN.0:JM),
                      TX1(0:IN.0:JM) - TY1(0:IN.0:JM) -
     2
                      TX2(0:IM.0:JH), TY2(0:IH,0:JH),
     3
                      TAUX (0: IN. 0: JH) . TAUY (0: IN. 0: JH) .
                      TAUX1(0:1H.0:JH), TAUX2(0:1H.0:JH),
                      TAUY1(0:IM.0:JM): TAUY2(0:IM.0:JM):
                      WADX1 (NATINDS) . WADX2 (NATINDS) .
                      WHENTY I (MICHIES) . WHENTY I (NHINTES) . WSPD (IC1. JC1) .
                      IDAY1, IHOUR1, TIME1, IDAY2, IHOUR2, TIME2,
                      RHDAIR, WCDMVF,TXF(0:IM,0:JM),TYF(0:IM,0:JM),
                      TXFL (0: IN.O: JH) . TYFL (0: IN.O: JH)
      CONTON /BLK33/ ITEST, IPA, IPB, ID, JPA, JPB, JD
      CONTION /BLK34/ FNAN(ICELLS, JCELLS), COR, SR, CTB, ROI, CZMULT
      ECHPION /BLK35/ 161: 164: 16T: 16S: 16U: 16W: 16C: 169: 16P
      CONTON /BLK36/ IFI, IFD, IFDS,
                      IMQ. IPT. IVIS
      CURPEN /BLK37/ IT, IDAYO, IHDURO, IMINO, ISEDO, ITI, IT2, TIME,
                      TIMES, TIMEO, ITWOS, ITSALT, TIMSEC, TIMEA, TIMEB,
     1
     2
                      TIMEC, TIMED, IDAYTI, IHRTI, IDAYT2, IHRT2,
                      TIMETI, TIMET2, TEP2, TEX2, ITPTS
      CONTON /BLK38/ ININD
      CONTION /BLK39/ IBTH, H1, H2, HAZD, HMIN, SSSO, XMAP
      CONTION /BLK39A/ A1(IJMAX), A2(IJMAX), A3(IJMAX), A4(IJMAX),
                      B1(IJMAX), B2(IJMAX), B3(IJMAX), B4(IJMAX),
                      AA(IJHAX), BB(IJHAX), CC(IJHAX), DD(IJHAX)
      CHARACTER+4 NEX (ICELS, JCELS), NEY (ICELS, JCELS)
      CONTON /BLX40/ NBX, NBY
C
      COMMON /PFLAG/ IPSW, IPUIN, IPVIN, IPSSW, IPUM, IPVW,
     1
                      IPSG, IPUIG, IPVIG, IPSSG, IPUG, IPVG,
     2
                      IPWW, IPSAW, IPTEW, IPROW,
     3
                      IPMG, IPSAG, IPTEG, IPROG
      CORRIGH /TRN01/
                        6D(0: IM.0: JM.3)
      COMMON /TRN02/ 611(0:1H-0:JH-3), 612(0:1H-0:JH-3).
                       622(0: IM, 0: JM, 3)
```

```
COMMON /TRN03/ H11(0:1H,0:JH,3), H12(0:1H,0:JH,3),
                       H22(0: IN. 0: JM. 3)
       COMMON /TRN04/ D111(0:IM.0:3M.3), D112(0:IM.0:3M.3),
                      D122(0:1H,0:JH,3)
      EDMMON /TRNO5/ D211(0:IH.0:3H.3), D212(0:IH.0:3H.3),
                      D222(0:1M, 0:3M, 3)
      COMMON /TRN07/ FX11(0:1H,0:JH), FX12(0:1H,0:JH),
                      FX21(0:IM.0:JM), FX22(0:IM.0:JM)
      CONTON /TRNOS/ FY11 (0:1M-0:3H) . FY12 (0:1M-0:3H) .
                      FY21 (0: IN. 0: JH) , FY22 (0: IN. 0: JH)
      COMMON /TRNO9/ X1U(IC1.JC1).X2U(IC1.JC1).Y1U(IC1.JC1).Y2U(IC1.JC1)
      COMMON /TRN10/ X1V(IC1, JC1), X2V(IC1, JC1), Y1V(IC1, JC1), Y2V(IC1, JC1)
      COMMON /TRN11/ X1C(IC1-JC1).X2C(IC1-JC1).Y1C(IC1-JC1).Y2C(IC1-JC1)
      COMMON /TRN12/ X1 (IC1.JC1).X2 (IC1.JC1).Y1 (IC1.JC1).Y2 (IC1.JC1)
      CONTION /AREA01/ XCT(IC1.JC1). XCXX(IC1.JC1). XCYY(IC1.JC1).
                       XCXXYY (IC1, JC1)
      COMMON /AREA02/ YCT(IC1.JC1), YCXX(IC1.JC1), YCYY(IC1.JC1).
                       YCXXYY(IC1, JC1)
C
       COMMON /ADDOL/ FMU(IC1): FMV(JC1): FMS(IC1): FMSV(JC1)
C
      CONTION /ADDOZ/ SG(KH), DZZ(KH), Z(KH), DZA(KH), DZB(KH)
      COMMON JADDOS/ U(0:1H-0:JH-KM) . UN(0:IM-0:JH-KM) . UN(0:IM-0:JH-KM)
      COMMON /ADDO4/ V(0:IN-0:JH-KH). VN(0:IN-0:JH-KH). VN(0:IN-0:JH-KH)
      COMMON /ADDOS/ W(O:IM.O:JM.KH)。編(O:IM.O:JM.KH)。MN(O:IM.O:JM.KH)
     1
                     .WT (0: IH. 0: JH) . LISAV (0: IH. 0: JH. KH) . V3AV (0: IH. 0: JH. KH)
      COMMON /ADDO6/ FBC(0:IM.0:JM),
                                          FBCV(0:IM.0:JM),
                      FI (0:1M.0:JM.KM), FJ
                                              (0: IN. 0: JM. KM) .
     1
                      FRO (0: IM. 0: JM. KM) . FDABC (0: IM. 0: JM. KM) .
     2
                      FRQ(0:IN,0:JM,KM), FQABC(0:IN,0:JM,KM),
     3
                      FXYZ (0: IN. 0: JM. KM)
      COMMEN /ADDOT/ C (0:1H.0:JH.KH), CA(0:1H.0:JH), CEQ(0:1H.0:JH),
     1
                      T (0:1M.0:JM.KH). TN (0:1M.0:JM.KH).
     2
                      SA(0:IN.0:JM.KH), SAAV(0:IN.0:JM.KH),
     3
                      SAU(0:IM.0:JM.KH).JS1(IM), JS2(IM), FSUH, SAINT
      COMMON /ADD7A/ IDAYS1, IHRS1, TIMES1, IDAYS2, IHRS2, TIMES2,
     1
                      SAI (NTIDES: IJHAX: KH): SAZ (NTIDES: IJHAX: KH):
     2
                      TEL (NTIDES, IJMAX, KM), TEZ (NTIDES, IJMAX, KM)
      COMMON /ADDOTB/ IDYTE1, IMRTE1, TIMTE1, IDYTE2, IMRTE2, TIMTE2,
     1
                      TE3(NRIVRS, IJHAX, KH), TE4(NRIVRS, IJHAX, KH),
     2
                      SAJ (NRIVRS, IJMAX, KH), SA4 (NRIVRS, IJMAX, KH)
      CONTON /ADDOB/ R(0:IM.0:JM.KM). RU(0:IM.0:JM.KM).RV(0:IM.0:JM.KM).
     1
                     RS(0:1M.0:JM), RUS(0:1M.0:JM), RVS(0:1M.0:JM)
     CONTON /ADDOG/ GA (O:IM.O:JM.KM), GB (O:IM.O:JM.KM).
     1
                     EAB( 0:IM.0:JM), EBB( 0:IM.0:JM),
     2
                     RIA(O:IM.O:JM.KM) . RIB(O:IM.O:JM.KM) .
     3
                     VELGA(O: IN.O: JM.KH) . VELGB(O: IN.O: JM.KH)
     CONTRON /ADDIO/ QQQ(O:IM.O:JM.KM), SL (O:IM.O:JM.KM)
     COMMON /ADDII/ UIX (0:IM.0:JM), UIY (0:IM.0:JM), UIC(0:IM.0:JM),
     1
                     VIX (0:IM.0:JM), VIY (0:IM.0:JM), VIC(0:IM.0:JM),
    2
                     UC (0:IN.0:JM.KM), VC (0:IN.0:JM.KM)
     COMMON /ADD12/ URES(0:IN.O:JH.KM), VRES(0:IN.O:JH.KM),
    1
                     WRES (O: IN. O: JH. KH).
    2
                     UIRES (0: IN. 0: JM) . VIRES (0: IM. 0: JM) .
    3
                     TEXRS(0:IN.0:JM), TEYRS(0:IM.0:JM)
```

```
COMMON /ADDI3/ UIW(0:JM). UIE(0:JM). VIS(0:IM). VINN(0:IM).
                     SABE (KM), SABW (KM), SABS (KM), SABN (KM),
                     TBE (KM), TBW (KM), TBS (KM), TBN (KM),
                     CBE (KM), CBW (KM), CBS (KM), CBN (KM)
      COMMON /ADDI4/ TXC (0:IH.0:JH), TYC (0:IH.0:JH),
                     TX2C (0:1M.0:JM). TY2C (0:1M.0:JM).
     1
     2
                     FRICX(0:IM.0:JM). FRICY(0:IM.0:JM).
     3
                     BZO (0:IM.0:JM), BZOU (0:IM.0:JM)
C
      COMMON /INPO1/ XDIST(2*IN+1), XSLDPE(2*IN+1),
                     YDIST(2*JM+1), YSLOPE(2*IM+1),
                     XKAPPA (37-NTIDES) - XLONG (NTIDES)
      CORMON /INPOZ/ AVI, AVZ, BZI, CO, FKB, ZREFBN, ZREFTN, OMEGA
      CORMON /INPOS/ ICC1, ICC2, JCC1, JCC2, ID1, ID2, JD1, JD2,
                     IGRID, TOO, THE, THE,
                     TZ1, XDAY, "HOUR, XYEAR, XMONTH
C
      CONTION /ADDSO/ IVER, ICON, IUBO, IBL, IBR, JRM, JBP, CREF, CMAX
      CONTION /ADDS1/ XREF, ZREF, UREF, WREF, SREF, ROO, ROR, TO, TR
      CONMON /ADDS2/ IEXP, IAV, AVR, AHR, APA, AVREF, AVM, AVMI
      COMMON /ADD53/ IVLCY, ISALT, ICC, IFA, IFB, IFC
      CONTON /ADDSA/ IRD, IW, IWR, ICI, IR4, IWC, ICONC, IWS, IREAD, IRUN
      CONTON /ADDSS/ DZ, EH, EV, H, FR, FR2, FRD, FRD2, RB, RBV, BETA,
                     SZ, TAUR, WTS, WTU, MTV
      COMMON /ADDS6/ IP1, IP2, IP3, IPU, IPW, KPA, KPB, KD,
                     IGL, IGRI, IGTB, IRES, TRES
      CONTON /ADDS7/ ITEMP, TQ(0:IM,0:JM), BVR, S1, S2, PR, PRV
      CONTON /ADDS8/ NRANGE, KST (NSTATS)
      CONTON /ADDS9/ FHI, FH2, ZTOP, BSC, ZAB, TRII, TRI2, SQUI, SQUI,
                     Q2R1, MMX
      CONTION /ADD60/ ISHALL, ISIE, ITB
      COMMON /ADD61/ ATB, BTB, STB, VCB, WK, ZREFE, ZREFT, ZOT,
                     SLMIN, QOMIN
      CONTION /ADD62/ OCUT, ICUT, GAHAX, EBHAX, FZS, KSHALL
      COMMON /ADD63/ SSMAX, ISMAX, JSMAX, UUMAX, IUMAX, JUMAX, KUMAX,
                                          WHAX, IVHAX, JVHAX, KVHAX
      EDMMEN /ADD64/ DHX(0:IM.0:JM), DHY(0:IM.0:JM)
      COPPON /ADD65/ IX8(NX8PTS), IY8(NX8PTS), NX8,
                     JX8(NYBPTS), JY8(NYBPTS), NYB
      COMMON /ADD66/ NISS, ISS(ISSMAX), JSS(ISSMAX),
                     NDEPTH (NSDMAX), TDEPTH(NSDMAX),
                     ZDEPTH (NSDHAX, ISSMAX),
                     ZSAL
                             (NSDMAX.ISSMAX). SK(KH.ISSMAX)
      CONTON /ADD67/ SX(0:IM.0:JM). SY(0:IM.0:JM)
      CONTON /ADD68/ ACST(NCNST): PCST(NCNST)
      CORMON /ADD69/ TEP(0:1M.0:JM), TEX(0:1M.0:JM), HN(0:1M.0:JM)
C
      CONTON /HOOBJ/ AREA(0:IN.0:JM). DFAC(IC1.JC1)
E**** added for visualization Rao 7/29/93
      INTEGER VISSTRF, VISENOF, VISINTF, VISSTRS, VISENOS, VISINTS,
              VISSTRT, VISENOT, VISINTT
      CONMON /VIS/ VISSTRF, VISENOF, VISINTF, VISSTRS, VISENOS,
                   VISINTS, VISSTRT, VISENOT, VISINTT
C####
```

Appendix B List of Input Data in File 4

```
DUMMY
TITLE
         Run descriptor (Format A80)
DUMMY
IT1, IT2, DT, ISTART, ITEST, ITSALT (218,F8.0,418)
                   ; Starting time step ( always set = 1)
                   : Ending time step
   IT2
   DT
                   ; Computational time step in sec
                   ; Cold start
   ISTART = 0
                    Hot start (not operational)
      > 0
   ITEST = 0
                   ; No diagnostic output
                   : Diagnostic output
      > 0
                   ; Number of time steps after which salinity and
   ITSALT
                    temperature computations are initiated
DUMMY
WPRCRD (918,A8)
                   ; Number of print control lines which follow
   WPRCRD
DUMMY
WXCEL1, WXCEL2, WYCEL1, WYCEL2, WZCEL1, WZCEL2, WPRINT,
   WPRSTR, WPREND, WPRVAR (918,A8)
If WPRCRD > 0, WPRCRD lines have to be furnished below.
                   ; Starting \( \xi - cell \) index
    WXCEL1
                   ; Ending \(\xi\)-cell index
    XCEL2
                   ; Starting n-cell index
    WYCEL1
                   : Ending n-cell index
    WYCEL2
                   ; Starting sigma layer index
    WZCEL1
                   ; Ending sigma layer index
    WZCEL2
                   ; Printing interval (number of time steps)
    WPRINT
                   ; Time step when printing starts
    WPRSTR
                   ; Time step when printing ends
    WPREND
                     Character string indicating variables printed
    WPRVAR
```

Note: The following characters are used in WPRVAR for designating different variables.

E: Surface elevation (cm)

X: X-direction unit flow rate (cm²/sec)

Y: Y-direction unit flow rate (cm²/sec)

U: X-direction velocity (cm/sec)

V: Y-direction velocity (cm/sec)

W: Z-direction velocity (cm/sec)

S: Salinity (ppt)

T: Temperature (deg C)

A : Average velocity magnitude (cm/sec) and direction (measured clockwise from the true North, deg)

DUMMY

SNPCRD (918,A8)

SNPCRD; Number of snapshot control lines to follow

DUMMY

SXCEL1, SXCEL2, SYCEL1, SYCEL2, SZCEL1, SZCEL2, SNPINT, SNPSTR, SNPEND, SNPVAR (918,A8)

If SNPCRD > 0, SNPCRD lines have to be furnished below.

SXCEL1 ; Starting &-cell index

SXCEL2; Ending \(\xi\)-cell index

SYCEL1 ; Starting η-cell index

SYCEL2 ; Ending η-cell index

SZCEL1 ; Starting sigma layer index

SZCEL2 ; Ending sigma layer index

SNPINT ; Snapshot interval (number of time steps)

SNPSTR; Time step when snapshots start SNPEND; Time step when snapshots end

SNPVAR ; Character string indicating snapshot

variables (same notation is used as in

WPRVAR)

DUMMY

NRANG (918,A8)

NRANG; Number of ranges for computing discharges

DUMMY

RANGDR, RPOS1, RPOS2, RPOS3, RRNAME (7X,A1,318,A45)

If NRANG > 0, NRANG lines have to be furnished below.

RANGDR; Range direction (X for ξ and Y for η)

RPOS1 ; ξ (η) cell index of range line

RPOS2 ; Starting η (ξ) cell index for range RPOS3 ; Ending η (ξ) cell index for range

RRNAME; Range descriptor (name)

```
DUMMY
IGI, IGH, IGT, IGS, IGU, IGW, IGC, IGQ, IGP (1018): Printout flags. A
value of 1 turns printing on and 0 turns it off.
                    : Print arrays such as NS, MS, NR, MR, etc.
    IGI
                    : Print all depth arrays
    IGH
    IGT = 0
    IGS = 0
                    : Print restart arrays
    IGU = 0
    IGW = 0
                    ; Print grid coordinates and depths
    IGC
    IGQ = 0
    IGP
                    ; Save grid information in FILE 23 for plotting
                     snapshots
DUMMY
XREF, ZREF, UREF, COR, GR, ROO, ROR, TO, TR (10F8.0)
    XREF
                    ; Reference horizontal grid distance
                     (Maximum horizontal dimension divided by
                     number of cells in that direction, cm)
                    ; Reference depth (average depth in cm)
    ZREF
                    ; Reference horizontal velocity
    UREF
                     (average velocity in cm/sec)
    COR
                    ; Coriolis parameter
    GR
                    : Gravitational acceleration (cm/sec<sup>2</sup>)
                    : Minimum density expected (gm/cc)
    RO0
    ROR
                    ; Reference density (maximum expected) (gm/cc)
                    : Minimum temperature (Celsius)
    TO
    TR
                    ; Reference temperature (maximum expected)
                     (Celsius)
DUMMY
THETA (10F8.0)
    THETA
                    ; Time level weighting factor in computations
                     (A value of 1.0 was used in the Bight model)
DUMMY
ITEMP, ISALT, ICC, IFI, IFA, IFB, IFC, IFD (1018)
                    ; No computation of temperature
   ITEMP = 0
                    ; Compute temperature (use daily equilibrium
           =-1
                     temperature as river boundary temperature)
                    : Compute temperature (use time-varying
           =-2
                     temperature as river boundary temperature)
   ISALT = 0
                    ; No computation of salinity
                    ; Compute salinity, setting salinity and
           =-2
                     temperature at tidal boundaries
                    : Not used
   ICC
           = 0
    IFI
           = 1
                    ; Compute nonlinear (inertia) terms
           = 0
                    : No computation of nonlinear terms
    IFA
           = 0
                    : Not used
                    : Not used
    IFB
           = 0
```

IFC = 0 : Not used

IFD = 1 : Compute horizontal diffusion terms

= 0 : No computation of horizontal diffusion terms

DUMMY

IVIS, IWQ, IPT (1018)

IVIS = 1 ; Save information for subsequent visualization

= 0 ; Information for visualization is not saved

IWQ = 1 ; Save information for input to Water Quality Model

= 0 ; Information for input to Water Quality Model is

not saved

IPT = 1 ; Save information for input to the Particle

Tracking Model

= 0 ; Information for input to the Particle Tracking

Model is not saved

DUMMY

VISSTRF, VISENDF, VISINTF (1018) (to be supplied only if IVIS=1)

VISSTRF ; Starting time step (integer) for saving

information for flow (surface elevation and

horizontal velocities)

VISENDF ; Ending time step (integer) for saving

information for flow (surface elevation and horizontal

velocities)

VISINTF ; Time step interval (integer) for saving flow

information

DUMMY

VISSTRS, VISENDS, VISINTS (1018) (to be supplied only if IVIS=1)

VISSTRS; Starting time step (integer) for saving

salinity information

VISENDS ; Ending time step (integer) for saving

salinity information

VISINTS ; Time step interval (integer) for saving

salinity information

DUMMY

VISSTRT, VISENDT, VISINTT (1018) (to be supplied only if IVIS=1)

VISSTRT ; Starting time step (integer) for saving

temperature information

VISENDT ; Ending time step (integer) for saving

temperature information

VISINTT ; Time step interval (integer) for saving

temperature information

Note: The ending time step should be greater than the starting time step. If you want to save only some visualization information (e.g., flow) but not others (e.g., salinity), set VISSTRF and VISENDF to realistic values corresponding to the simulation but set VISTRS and VISENDS to values > IT2.

```
DUMMY
BVR, S1, S2, PR, PRV, TWE, TWH, FKB, TQ0 (10F8.0)
                   : Reference turbulent thermal eddy diffusivity
    BVR = 1.0
                     (not used)
                   ; Empirical constant used in computation of
    S1 = 10.0
                     simple variable vertical eddy viscosity
       = 3.33
                   ; Empirical constant used in computation of
                     simple variable vertical eddy diffusivity
    PR = 1.
                   : Turbulent Prandtl number
                   : Vertical turbulent Prandtl number
    PRV = 1.
    TWE
                   ; Temperature in the epilimnion (for computing
                     initial conditions)
                   : Temperature in the hypolimnion (for computing
    TWH
                     initial conditions)
    FKB
                   ; Vertical grid index of the initial thermocline location
                     (for computing initial conditions)
    TQ0 = 0.0
                   ; Initial surface heat flux (cal/cm²/sec)
Note: The initial conditions computed using TWE, TWH, and FKB are
overridden by FILE 17.
DUMMY
IVER, ICON, IUBO, IBL, IBR, JBM, JBP (1018)
   IVER = 2
   ICON = 3
   IUBO = 0
   IBL = 1
   IBR = ICELLS
   JBM = 1
   JBP = JCELLS
DUMMY
CREF, CMAX, C0 (10F8.0)
   CREF = 1.
   CMAX = 100.
   CO
          = 0.
DUMMY
ICC1, ICC2, JCC1, JCC2, ID1, ID2, JD1, JD2 (1018)
   ICC1 = 0
   ICC2 = 0
   JCC1 = 0
   JCC2 = 0
   ID1 = 0
   ID2 = 0
   JD1 = 0
   JD2 = 0
```

DUMMY

IEXP, IAV, AVR, AV1, AV2, AVM, AVM1, AHR (218,8F8.0)

: Vertical eddy coefficient flag **IEXP**

IEXP = 0 ; Constant eddy coefficient. Set ISPAC(9)=0.

=-1; Munk-Anderson type first order turbulence model. Richardson number dependent eddv coefficient with length scale linearly increasing from bottom and surface

=-2; Munk-Anderson type first order turbulence model. Richardson number dependent eddy coefficient with length scale linearly increasing from bottom to surface

=-3 : Second-order turbulence model

Note: For IEXP < 0, set ISPAC(9)=1.

IAV : Reference vertical eddy viscosity flag. IAV = 0 ; Input parameter AVR is used as reference eddy viscosity

= 1 : Reference vertical eddy viscosity is computed from AV1+TXY*AV2, where TXY is the total wind stress and AV1 and AV2 are input parameters (applies only for IWIND=0 and IWIND=1)

AVR ; Reference vertical eddy viscosity (cm²/sec) AV1 ; Background vertical eddy viscosity when wind

is zero (cm²/sec).

AV2 ; If IAV=1, unstratified vertical eddy viscosity is computed from AV1+TXY*AV2.

AVM ; Minimum allowable vertical eddy viscosity (cm²/sec)

AVM₁ ; Minimum allowable vertical eddy diffusivity (cm²/sec)

> ; Reference horizontal eddy viscosity or diffusivity (cm²/sec)

DUMMY

AHR

FM1, FM2, ZTOP, SLMIN, QQMIN (10F8.0)

FM1 ; Parameter in Richardson number dependent eddy

viscosity

; Parameter in Richardson number dependent eddy FM2

diffusivity

; Distance between the top of the computational ZTOP

domain and the free surface (cm). Used in

computing turbulence length scale.

SLMIN ; Minimum value of turbulence macroscale (cm)

QQMIN ; Minimum value of turbulent kinetic energy

(gm/cm/sec²)

```
DUMMY
ICUT, KSMALL, QCUT, GAMAX, GBMAX, FZS (218,8F8.0)
                   ; Eddy coefficients constant below halocline
   ICUT = 0
                   ; Eddy coefficients computed below halocline
         = 1
                   : Number of times eddy viscosity/diffusivity in
   KSMALL
                     turbulence model are smoothed (e.g., 5)
                   ; Coefficient in second-order turbulence model
   OCUT
                     (0.15 - 0.25)
                   : Maximum value of eddy viscosity (cm²/sec)
   GAMAX
                   ; Maximum value of eddy diffusivity (cm²/sec)
   GBMAX
                   ; Turbulence scale is not allowed to exceed the
   FZS
                     product of FZS and the depth
DUMMY
IWIND, TAUX, TAUY (18,5F8.0)
                   : Steady and uniform wind stress
   IWIND = 0
                   : Steady and uniform wind speed
           = 1
                   ; Steady and space variable wind stress
           = 2
                   ; Steady and space variable wind speed
           = 3
                   : Time variable and uniform wind stress
                   : Time variable and uniform wind speed
           = 5
                   : Time and space variable wind stress
          = 6
                   : Time and space variable wind speed
           = 7
   TAUX
                   : Uniform wind stress in x-direction if IWIND =0
                     Uniform wind speed in x-direction if IWIND=1
                   : Uniform wind stress in y-direction if IWIND =0
   TAUY
                     Uniform wind speed in y-direction if IWIND=1
DUMMY
ISPAC(I), I=1,10 (10I8)
   ISPAC(1) - ISPAC(3) = 0 (Not used)
                                   ; Flag for computing open boundary
   ISPAC(4)
                                    velocities
   ISPAC(5) - ISPAC(8) = 0 (Not used)
                                   : For IEXP = 0
                         = 0
   ISPAC(9)
                                   : For IEXP < 1
                         = 1
   ISPAC(10)
                         = 0 (Not used)
DUMMY
JSPAC(I), I=1,10 (1018)
   JSPAC(1) = 0 (Not used)
                   : Flag for 3-D mode, quadratic friction
   JSPAC(2)
              = 0 : Constant bottom friction factor = CTB
              = 1 ; Bottom friction based on logarithmic law
                   ; Flag for Coriolis terms
   JSPAC(3)
              = 0 ; Coriolis effects accounted for
              =-1 : Coriolis effects neglected
    JSPAC(4) - JSPAC(10) = 0 (Not used)
```

```
DUMMY
 RSPAC(I), I=1,10 (10F8.0)
     RSPAC(1) - RSPAC(6) = 0. (Not used)
     RSPAC(7)
                    ; Depth (cm) below which the bottom friction
                      coefficient follows a ramp function
    RSPAC(8)
                    ; Dummy parameter (set to 0.008)
    RSPAC(9) - RSPAC(10) = 0. (Not used)
DUMMY
IBTM, HADD, HMIN, H1, H2, SSS0, HMAX (18,5F8.0)
    IBTM
                    ; Bottom bathymetry flag
    IBTM = 0
                    ; Bottom depth varies linearly from west to
                      east of the basin
                    ; Bottom depth varies linearly from south to
                      north of the basin
                    ; Bottom depth array for cell center depths
          = 2
                      read from input file (FILE 4)
                    : Bottom depth arrays HS, HU, HV read from
          = 3
                      FILE 12
          = 4
                    ; Bottom depths and coordinates of cell corners
                      read from FILE 15 (set ITRAN=2)
    HADD
                    ; A constant depth added to the depth array
                      (cm)
    HMIN
                    ; Minimum water depth (cm)
                    ; Bottom depth (cm) along the west or south
    H1
                     boundary of the basin for IBTM = 0 or 1
    H2
                    ; Bottom depth (cm) along the east or north
                     boundary of the basin for IBTM = 0 or 1
    SSS0
                    ; Initial water surface elevation (cm)
    HMAX
                    ; Maximum water depth (cm) allowed
DUMMY
ISMALL, ISF, ITB, ZREFBN, CTB, BZ1, ZREFTN, TZ1 (318,7F8.0)
    ISMALL = 0
                   ; Small amplitude assumption is invoked.
                     Surface elevation is not added to the still
                     water depth to obtain the total depth
                    ; Small amplitude assumption is not invoked.
            = 1
                     Surface elevation is added to the still
                     water depth to obtain the total depth
   ISF
            = 0
                   : Free surface current flag (set to 0)
   ITB
                   : Bottom friction flag
                   ; Linear bottom friction for internal mode
            = 1
                   ; Quadratic bottom friction for internal mode
   ZREFBN
                   ; Reference height above bottom (cm)
   CTB
                   ; Constant bottom drag coefficient (typical
                     value 0.003)
   BZ1
                   ; Bottom roughness height (cm)
   ZREFTN
                   ; Reference height at the top (cm)
```

TZ1

; Constant surface roughness height (cm)

DUMMY

XMAP, ALXREF, ALYREF (10F8.0)

XMAP

: Mapping factor that scales the (x,y)

coordinates created by the grid generation

code to the real world

ALXREF

; X-reference length in the computational plane

ALYREF

; Y-reference length in the computational plane

Note: ALXREF and ALYREF are used if ITRAN = 0

DUMMY

ITRAN (1018)

ITRAN = 0

: Cartesian grid

= 1

; Curvilinear grid created by WESCOR. Cell corner coordinates read from FILE 15

= 2

: Curvilinear grid created by WESCORA or EAGLE.

Cell corner coordinates and depths read from

FILE 15

DUMMY

ITBRK(I), I=1,10 (1018)

ITBRK(I), I=1,10; Time steps at which information is written to

hot-start files (increasing order)

DUMMY

NSTA, NFREQ, NSTART (1018)

NSTA

: Number of stations where information is saved

for time series plots of currents

NFREQ

; Time step interval for saving currents

NSTART

; Beginning time step for saving currents

DUMMY

IST(K), JST(K), STATID(K) (214,A48)

If NSTA > 0, NSTA lines have to be furnished below.

IST(K), JST(K); Cell indices (I,J) of a station where

currents are saved

STATID(K)

: Station descriptor

DUMMY

NSTAS, NFREQS, NSTRTS (1018)

NSTAS

; Number of stations where water surface

elevations are saved for time series plots

NFREQS

: Time step interval for saving water surface

elevations

NSTRTS ; Beginning time step for saving water surface

elevations

DUMMY

ISTS(K), JSTS(K), STATS(K) (214,A48)

If NSTAS > 0, NSTAS lines have to be furnished below.

ISTS(K), JSTS(K)

; Cell indices (I,J) of a station where water

surface elevations are saved

STATS(K)

; Station descriptor

DUMMY

MSTA, MFREQ, MSTART (1018)

MSTA

; Number of stations where salinity and

temperature information is saved for time

series plots

MFREQ MSTART ; Time step interval for saving information

; Beginning time step for saving information

DUMMY

ISTSA(K), JSTSA(K), STATSA(K) (214,A48)

If MSTA > 0, MSTA lines have to be furnished below.

ISTSA(K), JSTSA(K)

; Cell indices (I,J) of a station where

salinity and temperature are saved

STATSA(K)

; Station descriptor

DUMMY

NRIVER

; Number of river boundaries (218,F8.0,418)

NRIVER = 0

: No river boundaries

< 0

; River inflows are steady

> 0

; Time variable inflows

If NRIVER = 0, use the following lines

DUMMY

DUMMY

If NRIVER > 0, use the following lines

DUMMY

IJRDIR(K), IJRROW(K), IJRSTR(K), IJREND(K)* (1018)

IJRDIR(K) = 1 ; River boundary is on left (west)

= 2

; River boundary is on bottom (south)

= 3

; River boundary is on right (east)

= 4

; River boundary is on top (north)

; Index of the row (J) or column (I) IJRROW(K) of the river boundary : Starting I or J index of the river boundary IJRSTR(K) ; Ending I or J index of the river boundary IJREND(K) * NRIVER lines have to be furnished If NRIVER < 0, use the following lines DUMMY JRDIR(K), JRROW(K), JRSTR(K), JREND(K)* (1018) IJRDIR(K) = 1 ; River boundary is on left (west)
= 2 ; River boundary is on bottom (south)
= 3 ; River boundary is on right (east)
= 4 ; River boundary is on top (north) ; Index of the row (J) or column (I) IJRROW(K) of the river boundary ; Starting I or J index of the river boundary IJRSTR(K) ; Ending I or J index of the river boundary IJREND(K) *INRIVER| lines have to be furnished followed by the lines shown below. DUMMY ICELL, JCELL, QRIVER(K,IJ)* (218,F8.0,418) ICELL, JCELL ; Coordinates of a cell (I,J) where QRIVER is prescribed QRIVER(K,IJ) ; Steady river inflow *Repeat for all the river cells, in order. DUMMY NBAR (1018) ; Number of interior thin-wall barriers NBAR If NBAR = 0, use the following line DUMMY If NBAR > 0, use the following lines **DUMMY** IJBDIR(K), IJBROW(K), IJBSTR(K), IJBEND(K)* (1018) IJBDIR(K) = 1 ; Barrier is in ξ -direction = 2 ; Barrier is in η-direction

IJBROW(K) ; Index of row (J) or column (I) of barrier

IJBSTR(K) ; Starting I or J index of barrier

IJBEND(K) ; Ending I or J index of barrier *NBAR lines have to be furnished.

DUMMY TIDFNO, TIDBND (1018) : Number of tidal elevation tables entered as TIDFNO input ; Number of tidal elevation boundaries TIDBND **DUMMY** If TIDFNO > 0, read the following line(s) TIDSTR(I), I=1, TIDFNO (1018) ; The entry number in each tidal elevation TIDSTR(I) table corresponding to the starting time of the simulation DUMMY If TIDBND > 0, TIDBND lines of the following format have to be read. IJDIR(I), IJROW(I), IJSTR(I), IJEND(I), TIDTYP(I), TIDFN1(I), TIDFN2(I) (418,A8,518) ; Tidal boundary is on left (west) IJDIR(I) = 1: Tidal boundary is on bottom (south) = 2 ; Tidal boundary is on right (east) = 3 : Tidal boundary is on top (north) = 4 ; Index of the row (J) or column (I) of the IJROW(I) tidal boundary : Starting I or J index of the tidal boundary IJSTR(I) ; Ending I or J index of the tidal boundary IJEND(I) TIDTYP(I) = "CONSTANT" ; Constant tidal elevation between IJSTR(I) and IJEND(I) = "INTERP" ; Linear interpolation of tidal elevation between IJSTR(I) and IJEND(I) ; The number of the tidal elevation table for TIDFN1(I) CONSTANT or INTERP type of boundaries : The number of the second tidal elevation TIDFN2(I) table used for interpolation on INTERP type boundaries Optional input: DUMMY ; Indices of a cell where HS is reset to 0. i, J (4x, 12, 1x, 12)DUMMY ; Indices of a cell where HU is reset to 0. I,J (4x,12,1x,12) DUMMY : Indices of a cell where HV is reset to 0. I,J (4x,12,1x,12) DUMMY I,J, RDEPTH (free format); Indices and depth (ft) of a cell where HS is reset to non-zero value RDEPTH.

Appendix C List of Input Data Files¹

FILE 13

River inflows are read from FILE 13. These data are read first as a time line (DAY and HOUR) formatted by 218. Next, the (I,J) location and discharge in cubic feet per second for each cell of each river boundary are read and formatted by (218, F8.0).

FILE 14

Wind data are read from FILE 14. These data are in the form of time (DAY and HOUR) and the x and y components of the wind velocity in meters per second of each wind field used. These data are formatted by (215,6F10.0).

FILE 15

The (x,y) coordinates and depths of the New York Bight grid cell corners are read from FILE 15. This file was created from a run of the grid generation code EAGLE and a depth interpolation program. The first line contains the file name formatted as A80. The number of corner points in ξ and η are read next unformatted. The coordinates and depths are read next unformatted, one line per corner.

FILE 16

Tabular tide data are read from FILE 16. The first line is the title formatted as A80. The tide data are in the form of time (MONTH, DAY, YEAR, HOUR, MINUTES) and the water surface elevations in centimeters relative to selected datum for TIDFNO points. These data are formatted by (I2,1X,2I3,1X,2I2,(T17,8F8.2)).

¹ A table of factors for converting non-SI units of measurement to SI (metric) units is presented on page vi.

FILE 17

The initial temperature field in degrees Celsius is read from FILE 17 by format (10E12.5). This file is created from a few observed values. The resulting field is then smoothed in the ξ and η directions several times before it is written to FILE 17.

FILE 18

The Manning's roughness n is hard-wired in the model for the New York Bight application. By changing the source code, a field of Manning's n values may be input by format (20F4.0). The input values are multiplied by 0.001 in the source code to yield the actual values. They are input by rows.

FILE 19

Daily average equilibrium temperatures in degrees Celsius and surface heat exchange coefficients in units of cm/sec are read from FILE 19. These data are in the form of time (DAY and HOUR), equilibrium temperature, and heat exchange coefficient. They are formatted by (215,F10.0,E12.5).

FILE 74

The initial salinity field in parts per thousand is read from FILE 74 by format (10E12.5). This file is created in the same fashion as FILE 17.

FILE 76

Time-varying salinity in parts per thousand and temperature in degrees Celsius at tidal boundaries are read from FILE 76 if salinity and temperature are to be computed. These data are in the form of time (DAY and HOUR) formatted by (215). Next, the (I,J) location of each tidal boundary cell and the vertical distribution of salinity, starting from the top layer to the bottom layer are read. These data are followed by temperature data using the same format as for the salinity. The format is (215,11F5.0)

FILE 78

Time-varying temperature data at river flow boundaries are read from FILE 78 if temperatures are to be computed and equilibrium temperatures are not used as river boundary temperatures. These data are in the form of a time (DAY and HOUR) formatted by (2I5). Next, the (I,J) location of river flow boundary cells and corresponding temperatures starting from top layer to bottom layer are read. These data are formatted by (2I5,11F6.0).

FILE 85

This file contains corner point information for the water quality boxes (free formatted).

FILE 90

This one line file contains the time averaging interval (NAVG) and the starting time step (ITPTS) for saving information for input to the Particle Tracking Model (free formatted).

FILE 95

This file contains the number of surface boxes (NSB), the time averaging interval (NAVG), the time step to start saving information (ITWQS), WQMINT, WQMSTR, WQMEND, and WQMSNP (free format). It also has information on each of the surface boxes and each flow face.

Appendix D Input Data in File 4 for April 1976 Application

```
TITLE (ABO)
   MY BIGHT TEST: 76 X 45 GRID RERUN 18; IFD = 1; 3-D sa &te 30days 8-13-73
    171
             172
                     DT ISTART
                                   ITEST ITSALT
           17280
                  150.0
 MPRCR0
 WICE 1
         WXCEL2 WYCEL1 WYCEL2 WZCEL1 WZCEL2 WPRINT
                              45
                                              10
                                                   17280
                                                                 1000000 EST
 SNPCRD
 SXCEL1 SXCEL2 SYCEL1 SYCEL2 SZCEL1 SZCEL2 SAPINT SAPSTR SAPENO SAPVAR
                                                           72900 100000 EST
      1
                              45
                                              10
                                                   17290
  NRANG
  RANGOR
                                 RRNANE
                                 EAST RIVER (MEST)
                      40
                                 EAST RIVER (EAST)
     161
             IEH
                     161
                             168
                                     IEU
                                             IGH
                                                     ΙŒ
                                                             162
                                                                     IP
                                                                       0
                                       0
                                                                      TR
            ZREF
                    UREF
                             OF.
                                             RDO
                                                     ROR
 521500.
           9144.
                                   981.0
                                                   1,021
                                                                     35.
   THETA
     1.0
   ITEP
           ISALT
                     IΩ
                             IFI
                                     IFA
                                                     IFC
                                                                     AH0
                                             1FB
                                                               1 100000.
      -2
                       0
                                                       0
             -2
    IVIS
VISSTRE VISENDE VISINTE
 VISSTRS VISEKOS VISINTS
 VISSTRT VISEROT VISINTT
                                                                     150
                                     PRV
    BVR
                              PR
     1.0
             10.
                                     1.0
                                                     10.
                                                                     0.0
    IVER
            ICON
                    TUBO
                                     IBR
                                             JEN
                             IR.
      2
    CREF
            DAI
                      \alpha
            100.
    IICI
             IC2
                    JJC1
                                     ID1
                                             102
                                                             J02
                                                               0
```

```
IEXP
            IAV
                   AVR
                           AV1
                                   AV2
                                           AVN
                                                  AVM1
                                                           AHR
    -3
                   10.
                            0.
                                    0.
                                           10.0
                                                 0.005 100000.
    FILL
            FH2
                  ZTOP
                          SLHIN
                                  NIMDO
    -.5
           -1.5
                    0.
                            1.
                                   0.01
   IDIT
        KSHALL
                  QCUT
                         GAHAX
                                 GEMAX
                                           FZS
     0
             0
                  0.15
                         5000.
                                 5000.
                                           0.2
 IMIMD
          TAUX
                  TAUY
     5
          0.00
                  0.00
  ISPAC(I), I=1,10
                             1
                                             0
                                                     1
                                                                     1
                                                                             0
  JSPAC(I) . I=1.10
     1 -
             1
                                             0
                                                     0
                                                                             0
  RSPAC(I), I=1,10
  .020
            0.
                .00001
                       -00001
                                    0.
                                            1.
                                                 1000.
                                                         0.008
                                                                   .25
                                                                           4.
  IBTH
          HADD
                 HMIN
                           HI
                                    H2
                                          SSS0
                                                 HIAX
                 304.8
            0.
                           0.0
                                   0.0
                                           0.0 999999.
ISHALL
           ISF
                   ITB
                       ZREFEN
                                   CTB
                                           BZ1 ZREFDN
                                                           TZ1
             ٥
                     5
                                0.0025
                                        0.005
                                                    5.
                                                            .2
 XMAP ALXREF ALYREF
30.48 521500 747400
ITRAN IBD(1)
                  (2)
                          (3)
                                  (4)
  ITERK (1)
               (2)
                       (3)
                               (4)
                                       (5)
                                               (6)
                                                       (7)
                                                               (8)
                                                                       (9)
                                                                              (10)
     70272
             88128 105408
                                0
                                        0
                                                 0
                                                                0
                                                                        0
                                                                                O
      NSTA
             NFRED INSTART
                             (CURRENT STATIONS)
         8
                48
                         0
   IST JST STATID(K)
                                     ( DNE CARD FOR EACH STATION )
                         (214,A48)
    37 15 MESA LT 1
    7 15 HESA LT 2
    11
        6 MESA LT 3
    54 17 HESA LT 4
   52
        9 MESA LT 5
   23 24 HESA LT 6
   40 42 HUDSON R. (40,42)
   38 41
          HUDSON R. (38,41)
    NSTAS
           NFREQS NSTRTS (TIDE STATIONS)
       13
               48
  IST JST
           STATID(K)
                        (214.A48)
                                     ( ONE CARD FOR EACH STATION )
           ATLANTIC CITY (4.25)
    4 25
   27
       37
           SANDY HOOK (27,37)
   39 41 THE BATTERY (39,41)
   62 37 NEW LONDON (62,37)
   68 43 NEWPORT (68,43)
   40 42 HUDSON R. (40,42)
   38 41 HUDSON R. (38,41)
       41 L.I. SOUND (44,41)
   44
   33
       7
           OCEAN BORY (33.7)
   73
      33
            (75.33)
   74
      33
            (74,33)
  75 33
            (73,33)
   75 31
            (75.31)
    HSTA
           HFREQ MSTART
                              (SALINITY STATIONS)
       7
             144
                    2880
 IST JST STATID(K)
                       (214.A48)
                                    ( ONE CARD FOR EACH STATION )
  37 15 HESA LT 1 (37,15)
   7 15 HESA LT 2 (7,15)
  11 6 HESA LT 3 (11,6)
```

```
54 17 HESA LT 4 (54,17)
   9 HESA LT 5 (52,9)
23 24 NESA LT 6 (23,24)
26 15 MESA LT 7 (26:15)
NRIVER
                                  ( DNE CARD FOR EACH RIVER )
IJRDIR IJRROW IJRSTR IJREND
                            42
     3
            40
                    42
                                  ( DNE CARD FOR EACH CELL )
             J ORIVER
     I
  NBAR
                                  ( DNE CARD FOR EACH BAR )
 IJRDIR IJRROM IJRSTR IJREND
 TIDENO TIDEND
     11
                                                                            10
                                                             8
              2
                      3
 TIDSTR
                                                                     1
      1
                          IJENO TIDTYP TIDENI TIDEN2
          IJROW IJSTRT
  IJDIR
                              6INTERP
      1
                                                      2
                                              3
                              BINTERP
      1
                                              2
                             25INTERP
      1
                                                      5
      2
                             10INTERP
                                                      6
                                              5
      2
                     10
                             32INTERP
                                                      7
                             60INTERP
      2
                     32
                                                      7
                                              7
                             761NTERP
      2
                     60
      3
                             43INTERP
                                                     11
              76
RESET HS(I.J) TO ZERO AT THE FOLLOWING CELLS
   24,45
    61.26
    62,26
    63,27
    58,30
    59,30
    66,30
    59,31
    60,32
    52,33
    26.36
    27.36
    71,36
    28,37
    34.37
    35,37
    64.37
    71.37
    72,37
     62,38
    72,38
     35,39
     44.39
     45,39
     46,39
     47,39
     72,39
     72,40
     40,41
     41,41
```

```
42,41
     43,41
     35,42
     36:42
     41,42
     42,42
     43,42
     49.43
     50,43
    51,43
    52,43
    53,43
    54.43
    56,43
RESET HU(1.J) TO ZERO AT THE FOLLOWING CELLS
    61,26
    62,26
    59.30
    26,36
    27,36
    35,37
    36,37
    72,37
    63,38
    36.39
    44.39
    45,39
    46,39
    47.39
    41,41
    42,41
    43,41
    36,42
    42,42
    43,42
    50,43
    51,43
    52,43
    53,43
   54,43
   57,43
RESET HV(I, J) TO ZERO AT THE FOLLOWING CELLS
   59,31
   52.JJ
   71,37
   64,38
   72,38
   44,39
   45,39
   46.39
   47,39
   62,39
   72,39
   72,40
   35,43
   36,43
   49,44
   50,44
```

```
51,44
52,44
53,44
54,44
56,44
RESET HS(I,J) TO THE FOLLOWING DEPTHS
STORAGE AREAS
END OF DATA
END OF FILE
```

Appendix E River Inflows in File 13

```
Original Data Date 04/01/76
 40
         42 -55500.
         42 -99900.
         42 -80600.
         42 -66000.
         42 -53900.
        42 -46000.
40
        42 -40800.
40
        42 -36400.
 8
        42 -33100.
 9
40
        42 -31500.
10
40
        42 -31200.
11
40
        42 -30000.
12
40
        42 -27400.
13
40
        42 -24400.
14
        0
        42 -23400.
15
40
        42 -22900.
40
        42 -30000.
17
40
        42 -30800.
18
        42 -29000.
19
        42 -27200.
20
        42 -27100.
21
40
        42 -24400.
```

Appendix F Wind Data in File 14

0 0 -4.745 0.080 -5.165 5.655 -5.550 4.215 7.415 0 6 -5.825 3.270 -6.425 7.505 -4.215 7.415 0 12 -6.375 9.670 -7.420 7.255 -0.770 10.425 0 18 -2.690 10.980 2.320 4.315 6.340 4.720 1 0 -0.210 6.150 3.410 1.620 3.645 1.340 1 6 2.990 0.330 4.905 1.215 4.765 0.660 1 12 2.860 -1.620 3.035 -1.165 3.425 -1.765 1 18 2.440 -0.615 3.520 -1.640 4.515 -1.670 2 0 1.875 -2.640 3.325 -6.880 5.200 -6.595 2 6 5.800 -9.530 6.450 -10.430 7.610 -12.375 2 12 10.130 -11.370 9.830 -11.270 10.640 -12.970 2 18 12.450 -10.640 11.270 -7.200 12.295 -8.345 3 0 10.485 -9.780 9.9720 -7.315 12.700 -4.390 3 6 10.805 -9.065 7.970 -4.480 8.525 -6.940 3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.435 5 6 10.175 1.835 8.500 2.470 6.440 3.250 5 18 7.050 4.465 6.140 2.950 4.640 3.895 6 0 7.000 4.500 3.895 -2.485 3.520 3.495 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 12 4.330 -0.650 3.020 -0.285 0.395 6 12 4.330 -0.650 3.020 -0.285 0.395 7 0 4.250 -0.650 3.020 -0.285 0.395 7 0 4.250 -0.650 3.020 -0.285 0.395 8 12 -0.010 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -0.330 -0.795 -1.735 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.555 8 10 -1.340 1.220 -0.320 -0.795 -1.735 -2.840 -0.520 9 12 -0.520 -0.550 9.840 -10.315 -2.605 -1.790 9 12 2.725 -18.945 1.525 -1.5975 5.470 -15.945 9 18 9.625 -1.5805 9.840 -10.315 9.725 -12.490 1 1.0 4.850 -4.080 5.505 -9.045 6.545 0.125 1 1 0 6 5.220 -1.2870 4.600 -1.3.795 5.470 -15.945 1 1 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 1 1 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 1 1 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 1 1 1 0 5.695 -1.3.475 5.825 -1.2975 5.470 -15.945 1 1 1 1 0 6.695 -1.2870 9.775 -6.485 8.000 -5.585 1									
0 12 -6.375 9.670 -7.420 9.255 -0.770 10.425 0 18 -2.690 10.980 2.320 4.315 6.340 4.720 1 0 -0.210 6.150 3.410 1.620 3.645 1.340 1 6 2.990 0.330 4.905 1.215 4.765 0.660 1 12 2.860 -1.620 3.035 -1.165 3.425 -1.765 1 18 2.440 -0.615 3.520 -1.640 4.515 -1.670 2 0 1.875 -2.640 3.325 -6.880 5.200 -6.595 2 6 5.800 -9.530 6.450 -10.430 7.610 -12.375 2 12 10.130 -11.370 9.830 -11.270 10.640 -12.975 2 18 12.450 -10.640 11.270 -9.200 12.295 -8.345 3 0 10.885 -9.780 9.720 -7.315 12.700 -4.390 3 6 10.805 -9.085 7.970 -4.480 8.525 -6.940 3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 11.540 0.790 -5.300 2.740 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.435 5 18 7.050 4.465 6.140 2.950 4.610 3.285 6 0 7.000 4.500 5.485 3.520 3.955 7 0 4.250 -2.655 3.135 -1.885 -0.315 -2.605 7 6 0.685 -3.330 -0.330 -2.2480 -4.575 -2.245 7 12 -0.210 -0.320 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.355 -2.640 -0.770 -2.245 9 18 9.625 -15.805 9.800 -1.0315 -3.585 -2.110 1 0 13.475 -2.655 3.135 -1.885 -0.315 -2.605 1 0 13.475 -1.200 -1.315 -1.835 -0.350 -2.340 -0.550 1 1 2 2.725 -18.945 -0.335 -0.350 -1.350 -0.550 1 1 2 3.490 -1.220 -1.110 -1.240 -3.510 -0.550 1 2 4.350 -4.650 3.200 -4.515 0.510 -3.605 1 2 4.350 -4.650 3.200 -4.515 0.510 -3.505 1 3 4.000 -3.490 -3.585 -1.935 -5.885 -2.110 -7.475 -6.630 1 5 8 6 6 6 4.215 0.020 3.290 -2.855 -0.350 -0.350 -2.640 -0.770 -2.245 1 2 -0.210 -0.320 -0.795 -1.735 -5.885 -2.110 -7.475 -6.630 1 1 2 -0.710 -0.320 -0.795 -1.100 -1.7475 -6.635 -1.7790 1 1 2 -0.725 -1.8945 -1.525 -1.935 -5.885 -2.110 -7.475 -6.635 -1.1450 -1.1450 -1.140 -1.140 -3.510 -1.5945 -1.1450 -	0	0	-4.745	0.080	-5.165	5.655	-5.550	4.175	
0 18 -2.690 10.990 2.320 4.315 6.340 4.720 1 0 -0.210 6.150 3.410 1.620 3.645 1.340 1 6 2.990 0.330 4.905 1.215 4.765 0.660 1 12 2.860 -1.620 3.035 -1.164 4.515 -1.670 2 0 1.875 -2.640 3.325 -1.640 4.515 -1.670 2 0 1.875 -2.640 3.325 -6.880 5.200 -6.595 2 6 5.800 -9.530 6.450 -10.430 7.610 -12.375 2 12 10.130 -11.370 9.830 -11.270 10.640 -12.970 2 18 12.450 -10.640 11.270 -9.200 12.295 -8.345 3 0 10.485 -9.780 9.920 -7.315 12.700 -4.390 3 6 10.805 -9.065 7.970 -4.480 8.525 -6.940 3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.435 5 18 7.050 4.465 6.140 2.950 4.640 3.895 6 0 7.000 4.550 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.326 6 12 4.350 -0.650 3.290 -2.485 2.755 0.326 6 18 4.050 -4.355 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.355 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.885 0.700 -7.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.535 8 0 -3.490 1.240 -3.545 -1.935 -2.340 0.535 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -0.375 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.535 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -6.110 -7.495 -6.630 11 0 4.850 -4.030 -4.990 -6.13.785 1.145 -10.515 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	0	6	-5.825	3.270	-6.425	7.505	-4.215	7.415	
1 0	0	12	-6.375	9.670	-7.420	7.255	-0.770		
1 6 2.990 0.330 4.905 1.215 4.765 0.660 1 12 2.860 -1.620 3.035 -1.165 3.425 -1.765 1 18 2.440 -0.615 3.520 -1.640 4.515 -1.670 2 0 1.875 -2.640 3.325 -6.880 5.200 -6.595 2 6 5.800 -9.530 6.450 -10.430 7.610 -12.375 2 12 10.130 -11.370 9.830 -11.270 10.640 -12.272 2 18 12.450 -10.640 11.270 -9.200 12.295 -8.345 3 0 10.485 -9.780 9.920 -7.315 12.700 -4.390 3 6 10.805 -9.685 7.7970 -4.480 8.525 -6.940 3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.453 5 12 8.055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.486 2.755 0.260 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.865 -0.315 -2.605 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.865 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.733 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.555 9 12 -7.735 -9.410 -8.025 -1.1670 -0.505 10 0 13.495 -7.735 -9.840 -10.315 9.725 -1.1730 -2.245 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 0 4.850 -4.080 5.505 -9.045 6.545 0.1379 -1.249 11 0 4.850 -4.080 5.505 -9.045 6.545 0.1379 -1.249 11 10 4.850 -4.080 5.505 -9.045 6.545 0.125 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 1 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 1 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	0	18	-2.690	10.980			6.340		
1 12 2.860 -1.620 3.035 -1.165 3.425 -1.765 1 18 2.440 -0.615 3.520 -1.640 4.515 -1.670 2 0 1.875 -2.640 3.325 -6.889 5.200 -6.595 2 6 5.800 -9.530 6.450 -10.430 7.610 -12.375 2 12 10.130 -11.370 9.830 -11.270 10.640 -12.920 2 18 12.450 -10.640 11.270 -9.200 12.275 -8.345 3 0 10.485 -9.780 9.920 -7.315 12.700 -4.390 3 6 10.805 -9.065 7.970 -4.480 8.525 -6.940 3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 9.510 -7.545 5 12 8.055 2.210 7.205 2.130 6.440 3.425 5 18 7.050 4.465 6.140 2.950 4.640 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.855 0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.535 8 0 -3.490 1.240 -3.585 -1.935 -5.885 -2.110 10 6 15.765 0.400 5.985 1.525 -1.935 -5.885 -2.110 10 6 15.765 0.410 -8.025 -11.670 -6.065 -17.790 11 0 4.850 -4.080 5.505 -10.375 5.470 -1.549 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	I	0	-0.210	6.150	3.410	1.620	3.645	1.340	
1 18		6	2.990	0.330	4.905	1.215	4.765		
2 0 1.875		12	2.860	-1.620			3.425		
2 6 5.800	1	18	2.440	-0.615	3.520	-1.640	4.515	-1.670	
2 12 10.130 -11.370		0	1.875			-6.680	5.200		
2 18 12.450 -10.640 11.270 -7.200 12.275 -8.345 3 0 10.485 -7.780 9.720 -7.315 12.700 -4.390 3 6 10.805 -9.065 7.970 -4.480 8.525 -6.940 3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.555 8.750 1.455 5 6 10.175 1.835 8.500 2.470 6.440 3.250 5 12 8.055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.845 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.555 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510		6	5.800	-9.530	6.450				
3 0 10.885 -9.780 9.920 -7.315 12.700 -4.390 3 6 10.895 -9.065 7.970 -4.480 8.525 -6.940 3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.675 1.205 10.825 1.585 8.750 1.455 5 0 12.675 1.205 10.825 1.585 8.750 1.453 5 10		12	10.130	-11.370					
3 6 10.805 -9.065 7.970 -4.480 8.325 -6.940 3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 1 <td< td=""><td></td><td>18</td><td>12.450</td><td>-10.640</td><td>11.270</td><td>-9.200</td><td></td><td>-8.345</td><td></td></td<>		18	12.450	-10.640	11.270	-9.200		-8.345	
3 12 10.840 -4.395 4.210 -1.115 6.645 2.870 3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.740 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 0 12.695 1.205 10.825 1.525 8.750 1.440 3.250 5 <		0	10.485	-9.78 0	9.920			-4.390	
3 18 6.820 -0.280 0.280 -0.275 5.145 5.945 4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 0 12.695 1.205 10.825 1.585 8.750 1.453 5 1 2.8055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000		6		-9.065					
4 0 4.125 1.540 0.790 -5.300 2.940 1.825 4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 6 10.175 1.835 8.500 2.470 6.440 3.250 5 12 8.055 2.210 7.0440 3.445 3.50 3.50 4.400 3.445 5 18 7.050 4.455 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 </td <td></td> <td>12</td> <td>10.840</td> <td>-4.395</td> <td>4.210</td> <td>-1.115</td> <td></td> <td></td> <td></td>		12	10.840	-4.395	4.210	-1.115			
4 6 7.315 -5.945 5.585 -11.920 4.640 -8.580 4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 6 10.175 1.835 8.500 2.470 6.440 3.250 5 12 8.055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -2.455 3.135 -1.865 -0.315 -2.605 7		18	6.820	-0.280		-0.275	5.145		
4 12 11.105 -8.605 11.070 -10.585 6.700 -12.160 4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 6 10.175 1.835 8.500 2.470 6.440 3.250 5 12 8.055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -2.655 3.135 -1.845 -0.315 -2.605 7 0 4.250<									
4 18 14.455 -6.010 12.910 -5.980 9.510 -7.545 5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 6 10.175 1.835 8.500 2.470 6.440 3.250 5 12 8.055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.845 -0.315 -2.605 7 6 0.685		6	7.315	-5.94 5	5.585	-11,920	4.640		
5 0 12.695 1.205 10.825 1.585 8.750 1.455 5 6 10.175 1.835 8.500 2.470 6.440 3.250 5 12 8.055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.885 -0.315 -2.605 7 6 0.685		12		-8.605	11.070	-10.585			
5 6 10.175 1.835 8.500 2.470 6.440 3.250 5 12 8.055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.280 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.865 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920	i .	18	14.455	-6.010	12.910	-5.980	7.510	-7.545	
5 12 8.055 2.210 7.205 2.130 6.400 3.445 5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.845 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.555 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8		0		1.205					
5 18 7.050 4.465 6.140 2.950 4.610 3.895 6 0 7.000 4.500 5.485 3.520 3.955 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.865 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.555 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 <td></td> <td>6</td> <td>10.175</td> <td>1.835</td> <td></td> <td>2.470</td> <td>6.440</td> <td></td> <td></td>		6	10.175	1.835		2.470	6.440		
6 0 7.000 4.500 5.485 3.520 3.953 4.180 6 6 4.215 0.020 3.290 -2.485 2.755 0.260 6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.865 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.535 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	5	12	8.055	2.210	7.205		6.400		
6 4,215 0,020 3,290 -2,485 2,755 0,260 6 12 4,350 -0,650 3,020 -4,515 0,510 -3,050 6 18 4,050 -4,325 3,695 -5,050 0,990 -4,595 7 0 4,250 -2,655 3,135 -1,865 -0,315 -2,605 7 6 0,685 -3,330 -0,355 -2,640 -0,770 -2,245 7 12 -0,210 -0,320 -0,795 -1,735 -2,340 -0,520 7 18 -0,920 1,220 -1,110 -1,240 -3,510 0,555 8 0 -3,490 1,240 -3,565 -1,935 -5,885 -2,110 8 6 -6,495 -4,030 -4,490 -6,110 -7,495 -6,630 8 12 -10,660 -7,735 -9,020 -10,890 -10,200 -13,940 9 18 -	5	18	7.050	4.465			4.610		
6 12 4.350 -0.650 3.020 -4.515 0.510 -3.050 6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.865 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.555 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 <td>6</td> <td>0</td> <td>7.000</td> <td>4.500</td> <td></td> <td>3.520</td> <td>3.955</td> <td></td> <td></td>	6	0	7.000	4.500		3.520	3.955		
6 18 4.050 -4.325 3.695 -5.050 0.990 -4.595 7 0 4.250 -2.655 3.135 -1.865 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.535 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490	6	6	4.215						
7 0 4.250 -2.655 3.135 -1.865 -0.315 -2.605 7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.555 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	6	12	4.350	-0.650	3.020	-4.515			
7 6 0.685 -3.330 -0.355 -2.640 -0.770 -2.245 7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.535 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510		18		-4.325					
7 12 -0.210 -0.320 -0.795 -1.735 -2.340 -0.520 7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.535 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510		0	4.250		3.135				
7 18 -0.920 1.220 -1.110 -1.240 -3.510 0.555 8 0 -3.490 1.240 -3.565 -1.935 -5.885 -2.110 8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510									
8 0 -3,490 1,240 -3,565 -1,935 -5,885 -2,110 8 6 -6,495 -4,030 -4,490 -6,110 -7,495 -6,630 8 12 -10,660 -7,735 -9,020 -10,890 -10,200 -13,940 8 18 -11,420 -9,410 -8,025 -11,670 -6,065 -17,790 9 12 2,725 -18,945 1,525 -15,975 5,470 -15,945 9 18 9,625 -15,805 9,840 -10,315 9,725 -12,490 10 0 13,495 -2,725 11,695 -2,285 8,610 -7,430 10 6 15,765 0,410 12,635 1,810 13,730 2,500 11 0 4,850 -4,080 5,505 -9,045 6,545 0,125 11 6 5,220 -12,870 4,600 -13,785 1,145 -10,515 11 12 5,695 -13,495 5,825 -12,990 4,335 -14,300									
8 6 -6.495 -4.030 -4.490 -6.110 -7.495 -6.630 8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510 <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	1								
8 12 -10.660 -7.735 -9.020 -10.890 -10.200 -13.940 8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.295 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	l .								
8 18 -11.420 -9.410 -8.025 -11.670 -6.065 -17.790 9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.295 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	j .								
9 12 2.725 -18.945 1.525 -15.975 5.470 -15.945 9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.285 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	ł								
9 18 9.625 -15.805 9.840 -10.315 9.725 -12.490 10 0 13.495 -2.725 11.695 -2.295 8.610 -7.430 10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	ı								
10 0 13,495 -2.725 11.695 -2.285 8.610 -7.430 10 6 15,765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	1								
10 6 15.765 0.410 12.635 1.810 13.730 2.500 11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	1								
11 0 4.850 -4.080 5.505 -9.045 6.545 0.125 11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	1	0							
11 6 5.220 -12.870 4.600 -13.785 1.145 -10.515 11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	10	6	15.765						
11 12 5.695 -13.495 5.825 -12.990 4.335 -14.300 11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	11								
11 18 8.415 -10.445 9.600 -10.380 7.875 -10.510	I .								
	l .								
12 0 8.495 -6.250 9.775 -6.485 8.090 -5.595									
	12	0	8.495	-6.250	9,775	-6.485	8.080	-5.585	

Appendix G Cell Corner Coordinates and Depths in File 15¹

AND 74VAE DOLD OF	MODELLATTO ALD O	CLI DODUCE DESCRIPTION THE COMME
1	AUMITMATES RAW O	ell corner depths in feet
77 46 685640.00	0/300 00	2074 FO
712180.00	86328.00	2871.58
739020.00	134440.00	1102.72
1	175750.00	845.24
768800.00 794390.00	209820.00	1064.46
1	239720.00	811.28
919210.00 638940.00	262880.00	696.21
	284560.00	922.45
856720.00	302050.00	1050.65
870350.00	317240.00	1767.19
883560.00	328250.00	2042.94
894500.00	338370.00	1307.50
907120.00	348440.00	1464.82
920590.00	359190.00	1394.77
934740.00	370350.00	2398.77
949350.00	381260.00	1630.39
964000.00	391580.00	2198.52
979940.00	400390.00	1998.72
993410.00	409090.00	1601.43
1007400.00	417370.00	2024.36
1019600.00	425990.00	1485.39
1030700.00	433970.00	1898.15
1040500.00	441280.00	1662.43
1049300.00	447660.00	1643.20
1056500.00	453770.00	3408.01
1062200.00	459810.00	2390.16
1066700.00	465600.00	2530.58
1070900.00	471180.00	3874.83
1075700.00	476150.00	2357.38
1080400.00	480840.00	3540.52
1085600.00	485320.00	2694.58
1090700.00	490050.00	3637.25
1095900.00	494570.00	4632.64
1100200.00	477570.00	3921.73
1105400.00	501250.00	2999.45
1109500.00	509590.00	2682.54
1114300.00	514710.00	1953.10
1119200.00	519800.00	2162-94
1124300.00	524940.00	2647.65
1130300.00	530120.00	2342.08
1135900.00	538300,00	2228.55

¹ A table of factors for converting non-SI units of measurement to SI (metric) units is presented on page vi.

Appendix H Tabular Tide in File 16

	_							-			
Nei	New York Bight : 8 - Constituents Tide			4/01/76	- 9/30/	76					
4		1 76	0 0	0.00	0.00	0.00	0.00	2.00	0.00	0.00	0.00
				0.00	0.00	0.00					
4		1 76	030	-39.56	-34.41	-33.85	-32.72	-33.01	-30.86	-28.67	-26.86
				-25.85	-26.86	-31.15					
4		1 76	1 0	-49.44	-42.68	41.95	-40.35	-40.79	-38.45	-36.15	-35.05
				-35.19	-35,28	-41.09					
4		1 76	130	-55.99	-48.03	-47.19	-45.25	-45.79	-43.40	-41.12	-40.85
				-41.12	-41.30	-48.22					
4		1 76	2.0	~58.83	-50.14	-49.25	-47.13	-47.74	-45,43	-43.30	-43.92
				-44.30	-44.55	-52.12					
		1 76	230	-57.82	-49.94	-48.06	-45.92	-46.57	-44.46	-42.60	-44.10
					-44.37						
4		1 76	30	-53.04	-44.53	-43.74	-41.74	-42.40	-40.60	-39.10	-41.42
					-42,28						
4		1 76	330	-44.90	-37.26	-36.61	-34.90	-35,54	-34.15	-33.09	-36.10
					-37.00						
4	;	76	4.0	-33.92	-27.65	-27,19	-25.91	-26,49	-25.59	-25,01	-28,53
					-29.42						
4	1	1 76	430				-15.38	-15.89	-15.52	-15.43	-19-26
					-20.08					220 12	
4	1	76	5 0	-6.80		-4.20	~4,05	-4.48	-4.66	-5.03	-8.92
				-9.36		-11.09					4
4	1	76	530	7.56	8.05	7.79	7.32	6,97	6.26	5.47	1.77
				1.43	1.24	1.80					••••
4	1	1 76	6.0	21.12		18.99	17.92	17.65	16.46	15.32	12.06
				11.84		14.33			101 10		
4	:	1 76	630	33.01		28.69	27.08	26.88	25.28	23.89	21.29
				21.21		25.66					/
8		1 76	7 0	42.43		36.21	34.16	34.00	32.09	30.56	28.81
				29.87	28.91	35.02	511.10	51100	OLIV/	04100	20171
4		1 76	730	48.71		41.03	38.69	38,54	36.43	34.88	34.13
,				34.31	34.43	41.79	00,00	55557	UI 10	O 11.00	01110
4		1 76	8 0	51.45		42.83	40.33	40.19	37.99	36.54	36.87
	•			37.17		45.51		104.57	W		- Care/
4	1	1 76	830	50.51	42.50	41.48	33.99	39.83	36.67	35.43	36.85
	•		000	37.24	37.48	45.90	30.77	20103	20101	20173	30.00
Ä	,	1 74	90	45.87		37.06	34.76	34.55	32.56	31.61	34.08
-			, ,	34.54		43.01	31.70	471.44	32430	31.01	37.00
4	,	1 76	930	37.92	30.64	29.86	27.91	27.63	25.91	25.33	28.75
7		. 10	/JV	29.24	29.53	36.97	41.71	£/:03	List 75	20.00	TA 17
4	,	1 74	10 0	27.16		20.37	18.90	18.55	17.18	17.01	21.21
7		. /0	10 0			28.19	30. TC	10.77	17.10	17.01	21.21
		171	1070	21.70	21.98		9 7#	7.00	7 01	7 21	11 07
^		. /0	1030	14.33	9.52	9.20	8.34	7.90	6.94	7.21	11.97
				12.43	12.68	17.31					

Appendix I Initial Temperature Field in File 17

```
0.00000E+00 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02
0.12500E+02 0.12600E+02 0.12600E+02 0.12600E+02 0.12600E+02 0.12700E+02 0.12700E+02 0.12700E+02 0.12700E+02 0.12700E+02
0.12700E+02 0.12700E+02 0.12700E+02 0.12600E+02 0.12600E+02 0.12600E+02 0.12300E+02 0.12300E+02 0.11700E+02 0.79000E+01
0.83000E+01 0.84000E+01 0.98000E+01 0.11200E+02 0.12300E+02 0.12300E+02 0.11900E+02 0.12300E+02 0.12300E+02 0.12500E+02 0.12700E+02
0.12600E+02 0.12600E+02 0.12600E+02 0.12600E+02 0.12400E+02 0.12400E+02 0.12600E+02 0.12600E+02 0.12600E+02 0.12600E+02
0.12500E+02 0.12400E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12700E+02 0.12700E+02 0.12700E+02
0.12500E+02 0.12300E+02 0.12100E+02 0.11900E+02 0.11600E+02 0.11700E+02 0.11700E+02 0.11800E+02 0.12100E+02 0.12300E+02
0.12300E+02 0.12300E+02 0.12000E+02 0.11900E+02 0.12000E+02 0.12200E+02 0.12000E+02 0.00000E+00 0.00000E+00 0.12500E+02
0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.1250
0.12500E+02 0.12500E+02 0.12500E+02 0.12500E+02 0.12700E+02 0.12700E+02 0.12700E+02 0.12700E+02 0.12700E+02 0.12700E+02
0.12700E+02 0.12700E+02 0.12600E+02 0.12600E+02 0.12600E+02 0.12300E+02 0.12300E+02 0.12300E+02 0.19900E+02 0.97000E+01 0.83000E+01
0.84000E+01 0.98000E+01 0.11200E+02 0.12300E+02 0.12300E+02 0.11200E+02 0.12300E+02 0.12300E+02 0.12600E+02
0.12600E+02 0.12600E+02 0.12600E+02 0.12400E+02 0.12400E+02 0.12600E+02 0.1260
0.12400E+02 0.12500E+02 0.12600E+02 0.12600E+02 0.12500E+02 0.12600E+02 0.12500E+02 0.1250
0.12300E+02 0.12100E+02 0.11900E+02 0.11800E+02 0.11700E+02 0.11700E+02 0.11800E+02 0.12100E+02 0.12300E+02
0.12300E+02 0.12000E+02 0.11900E+02 0.12000E+02 0.12200E+02 0.12000E+02 0.12000E+02 0.12000E+02 0.12500E+02 0.12500E+02
0.12264E+02 0.12215E+02 0.12182E+02 0.12092E+02 0.11939E+02 0.11760E+02 0.11599E+02 0.11484E+02 0.11432E+02 0.11481E+02
0.11549E+02 0.11644E+02 0.11744E+02 0.11872E+02 0.11954E+02 0.12021E+02 0.12070E+02 0.12099E+02 0.12102E+02 0.12067E+02
0.11983E+02 0.11840E+02 0.11741E+02 0.11661E+02 0.11502E+02 0.11399E+02 0.10959E+02 0.98345E+01 0.89857E+01 0.90401E+01
 0.98101E+01 0.10688E+02 0.11395E+02 0.11593E+02 0.11593E+02 0.11893E+02 0.12111E+02 0.12213E+02 0.12217E+02 0.12237E+02
0.12241E+02 0.1222E+02 0.12142E+02 0.12152E+02 0.1225E+02 0.12238E+02 0.12244E+02 0.12241E+02 0.12227E+02 0.12180E+02 0.12154E+02
0.12220E+02 0.12288E+02 0.12316E+02 0.12322E+02 0.12411E+02 0.12493E+02 0.12510E+02 0.12459E+02 0.12373E+02 0.12233E+02
0.12059E+02 0.11899E+02 0.11790E+02 0.1171Œ+02 0.1171E+02 0.11802E+02 0.11980E+02 0.12099E+02 0.12098E+02 0.1205E+02
 0.11797E+02 0.11647E+02 0.1160XE+02 0.11644E+02 0.11700E+02 0.11700E+02 0.11700E+02 0.12500E+02 0.12500E+02 0.11591E+02
 0.116/FE+02 0.1170EE+02 0.1554E+02 0.11265E+02 0.10931E+02 0.10635E+02 0.10421E+02 0.10312E+02 0.10335E+02 0.10435E+02
 0.1466EE+02 0.10771E+02 0.10734E+02 0.11070E+02 0.11180E+02 0.11258E+02 0.1130EE+02 0.1130E+02 0.1125EE+02 0.11126E+02
 0.10756E+02 0.10511E+02 0.10711E+02 0.10624E+02 0.10534E+02 0.10215E+02 0.9579EE+01 0.91046E+01 0.91206E+01 0.956Z3E+01
 0.10141E+02 0.10657E+02 0.10940E+02 0.11119E+02 0.11363E+02 0.11555E+02 0.11681E+02 0.11755E+02 0.11817E+02 0.11855E+02
 0.11866E+02 0.11849E+02 0.11864E+02 0.11899E+02 0.11896E+02 0.11849E+02 0.11795E+02 0.11732E+02 0.11732E+02 0.11732E+02
 0.11781E+02 0.11838E+02 0.11920E+02 0.12057E+02 0.12192E+02 0.12278E+02 0.12300E+02 0.1225E+02 0.12168E+02 0.12039E+02
 0.11904E+02 0.11796E+02 0.11724E+02 0.11720E+02 0.11787E+02 0.11904E+02 0.11979E+02 0.11951E+02 0.11811E+02 0.11550E+02
 0.11300E+02 0.11123E+02 0.11044E+02 0.11100E+02 0.11100E+02 0.11100E+02 0.98000E+01 0.98000E+01 0.10643E+02 0.10997E+02
 0.110E2E+02 0.1088&E+02 0.1050E+02 0.10072E+02 0.98967E+01 0.941E7E+01 0.9253&E+01 0.9251BE+01 0.93940E+01 0.95955E+01
 0.97979E+01 0.99838E+01 0.10140E+02 0.10263E+02 0.10349E+02 0.10397E+02 0.10400E+02 0.10342E+02 0.10217E+02 0.10054E+02
 0.99105E+01 0.98215E+01 0.97765E+01 0.97243E+01 0.95321E+01 0.91794E+01 0.89102E+01 0.89119E+01 0.91783E+01 0.95740E+01
 0,99696E+01 0.10261E+02 0.1045Œ+02 0.10699E+02 0.10879E+02 0.11030E+02 0.11159E+02 0.11277E+02 0.11372E+02 0.11439E+02
 0.11476E+02 0.11504E+02 0.11506E+02 0.11452E+02 0.11348E+02 0.11213E+02 0.11080E+02 0.10992E+02 0.10985E+02 0.10986E+02
 0.11060E+02 0.11204E+02 0.11420E+02 0.11657E+02 0.11864E+02 0.12008E+02 0.12076E+02 0.12064E+02 0.11975E+02 0.11875E+02
  0.1179E+02 0.11730E+02 0.11719E+02 0.11770E+02 0.11854E+02 0.11891E+02 0.11809E+02 0.11576E+02 0.11217E+02 0.10843E+02
  0.10539E+02 0.10347E+02 0.10300E+02 0.10300E+02 0.10300E+02 0.90000E+01 0.90000E+01 0.98455E+01 0.10276E+02 0.10366E+02
  0.10133E+02 0.97121E+01 0.92597E+01 0.85774E+01 0.85865E+01 0.83416E+01 0.81888E+01 0.84736E+01 0.87350E+01 0.89619E+01
  0.915Z7E+01 0.93082E+01 0.94273E+01 0.95072E+01 0.95494E+01 0.95512E+01 0.95023E+01 0.94013E+01 0.92722E+01 0.91597E+01
```

Appendix J Equilibrium Temperature and Surface Heat Exchange Coefficient in File 19

```
0 5.92000 0.80782E-03
       0 9.50000 0.13752E-02
      0 11.78000 0.72274E-03
     0 9.41000 0.97871E-03
     0 10.89000 0.58029E-03
0 7.37000 0.12215E-02
     0 12.83000 0.66323E-03
 7 0 12.17000 0.71294E-03
8 0 10.90000 0.58627E-03
9 0 8.88000 0.90113E-03
10 0 8.79000 0.74807E-03
11 0 11.52000 0.86637E-03
12 0 2.64000 0.89744E-03
13 0 8,38000 0,75715E-03
14 0 14.23000 0.60228E-03
15 0 15.27000 0.60419E-03
16 0 16.29000 0.50118E-03
17 0 22.11000 0.56547E-03
18 0 18.25000 0.13458E-02
19 0 18.16000 0.10136E-02
20 0 21.89000 0.67685E-03
21 0 19.27000 0.72728E-03
22 0 16.35000 0.77030E-03
23 0 18.34000 0.97082E-03
24 0 12.60000 0.10420E-02
25 0 11.50000 0.11441E-02
26 0 10.30000 0.80017E-03
27 0 7.79000 0.10492E-02
28 0 11.09000 0.89434E-03
29 0 12.92000 0.84630E-03
30 0 17.57000 0.67063E-03
31 0 12.64000 0.11663E-02
32 0 16.89000 0.10174E-02
33 0 16.53000 0.88597E-03
34 0 11.00000 0.91083E-03
35 0 13.49000 0.99233E-03
     0 16.79000 0.98062E-03
37 0 16.29000 0.99567E-03
38 0 12.69000 0.92397E-03
      0 10.96000 0.95982E-03
     0 16.58000 0.91131E-03
```

Appendix K Time-Varying Vertical Distributions of Salinity and Temperature at the Ocean Boundary in File 76

Appendix L Time-Varying Vertical Distribution of Temperature at the River Boundary in File 78

```
      0
      0

      40
      42
      7.5
      7.55
      7.6
      7.59
      7.58
      7.56
      7.55
      7.54
      7.52
      7.51

      61
      0
      0
      40
      42
      17.2
      17.1
      17.0
      16.8
      16.8
      16.7
      16.6
      16.5
      16.5
      16.4

      122
      0
      0
      0
      22.7
      22.7
      22.7
      22.1
      21.2
      20.2
      18.5
      16.6

      153
      0
      0
      40
      42
      22.5
      21.6
      21.2
      21.0
      21.0
      21.0
      21.0
      21.0
      20.8
      20.6
      20.6

      163
      0

      40
      42
      22.5
      21.6
      21.2
      21.0
      21.0
      21.0
      21.0
      20.8
      20.6
      20.6
```

REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC20503.

E AND DATES COVERED
5. FUNDING NUMBERS
8. PERFORMING ORGANIZATION REPORT NUMBER Instruction Report CERC-95-2
10. SPONSORING/MONITORING AGENCY REPORT NUMBER
Springfield, VA 22161.
12b. DISTRIBUTION CODE
time-varying numerical hydrodynamic and rways Experiment Station. For this g with a boundary-fitted grid in the rified with the field data measured in April rodynamics and transport were modeled for quality model of the NY Bight, which merical model and its various features. tts of input data, various data files required,

14.	SUBJECT TERMS Feasibility study Hydrodynamics	Transport User's manual	15.	NUMBER OF PAGES 82	
	11) 01 00) 110111100	(0111011001		16.	PRICE CODE
17.	SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED	18. SECURITY CLASSIFIC OF THIS PAGE UNCLASSIFIED	CATION 19. SECURITY CLASSIFICATION OF ABSTRACT	20.	LIMITATION OF ABSTRACT

an example case simulating hydrodynamics and transport in the NY Bight for the month of April 1976.